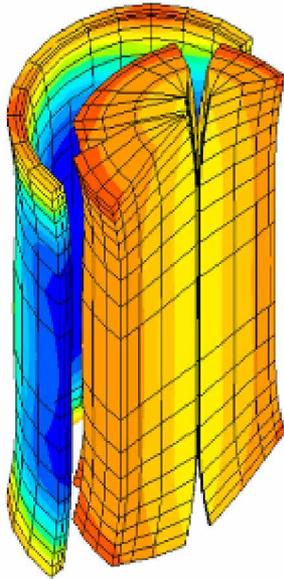


Exploratory research project:



Development of a manufacturing process for a  
simulating fuel for the study of fine fragmentation in  
LOCA

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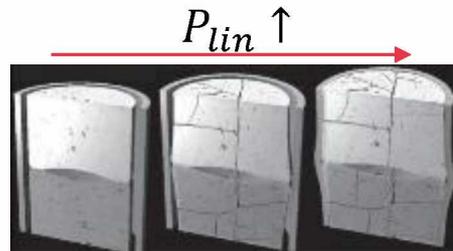
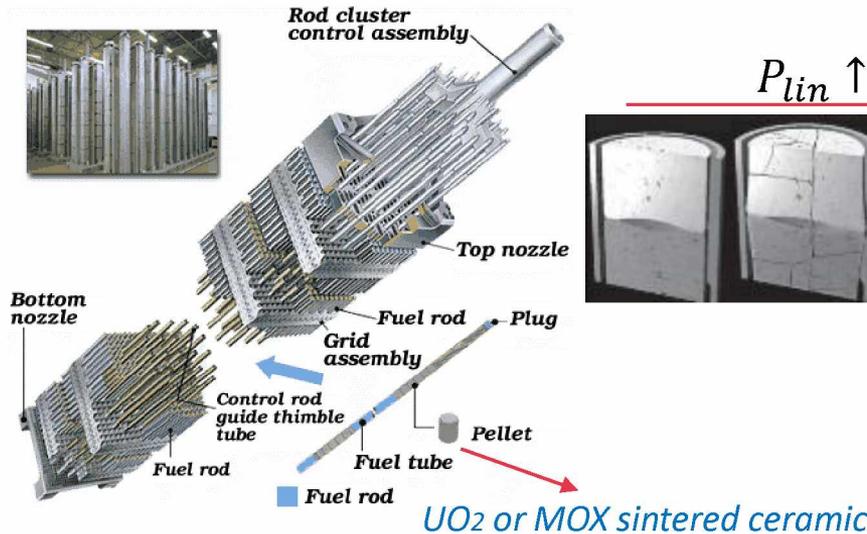
## Context of the study – fuel fragmentation

Fuel pellets undergo significant changes during their life in the reactor. Their condition is also potentially degraded during an incident or accident.

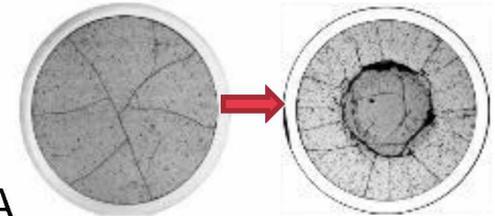
Fabrication

Base Irradiation

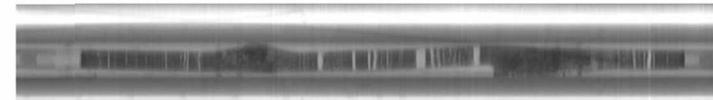
Incident/Accident



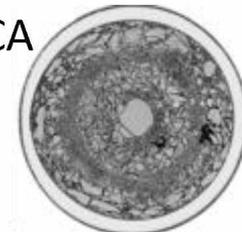
- Power ramp



- RIA



- LOCA



## Study Objectives – Simulating fuel

A few programs exist for the study of fragmentation on irradiated fuels:

- Many influential parameters: burnup, irradiation history, test conditions (temperature, pressure and quantity of gas in the rod,  $dT/dt$ )
- Few tests (expensive, material consuming)

The objective of the study is to develop a pre-fragmented fuel fabrication process to various degrees:

- Ability to have several pellets with various characteristics of fragmentation
- Use outside the hot cell and possibility of studying fragmentation, relocation and dispersion/ejection under many conditions (crushing of rod section, impact, 4-point bending, semi-integral tests)...

# Project structure

**PRE-FRAGMENTED PELLET DESIGN**



**FABRICATION BY 3D PRINTING**

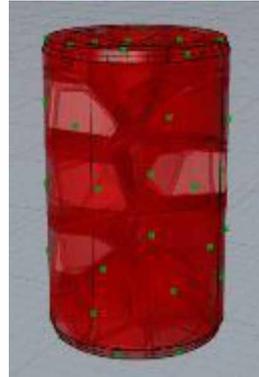


**EVALUATION OF THE MECHANICAL BEHAVIOR OF PELLETS**



## Main characteristics of model pellets

- CAD software used: Rhino7/Grasshopper
- Pellet geometry:
  - Modeling of dish and chamfers
  - External diameter: ~ 8.2 mm
  - Height ~ 13.5 mm
- Fragments: Points generation inside the pellet

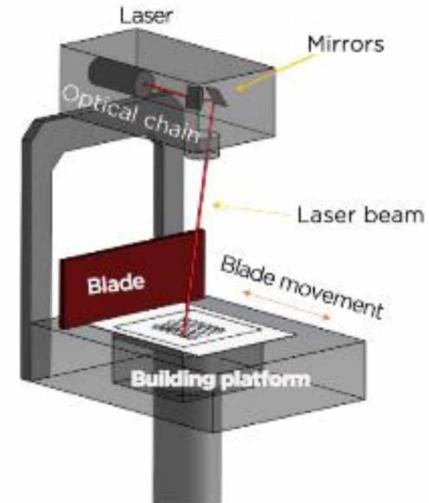


- IFZ (Inter-Fragments zone): "Brittle" but facilitating handling

# Direct printing by stereolithography

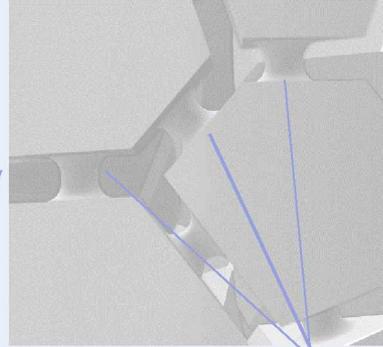
## Direct printing by stereolithography

- 3D CERAM C900 from Novadditive
- Resolution: ~ 0.035mm
- Fabrication without supports
- Material: Alumina  $\text{Al}_2\text{O}_3$
- Light-curing reaction of ceramic resin
- Debinding in air: removal of organic additives (1°C/min up to 600°C for 2 hours)
- Sintering: partial melting of the ceramic powder for densification (1700°C for 2 hours for maximum mechanical properties)



# 1. CAD model and validation in stereolithography printing

## CAD modeling with interconnected fragments



Fillets between fragments

### Pellet characteristics:

- 50 fragments of an average size of ~ 2 mm
- Distance between fragments: 0.4 mm
- Diameter of the bridges: 0.4 mm
- 0.2 mm fillets on bridges to prevent crack formation

## Feasibility test with Novadditive

Fabrication of two pellets



## 2. Lateral compression test

### Hertz model:

- Maximum stress is at the center of the disc and corresponds to a tensile stress along the x axis.

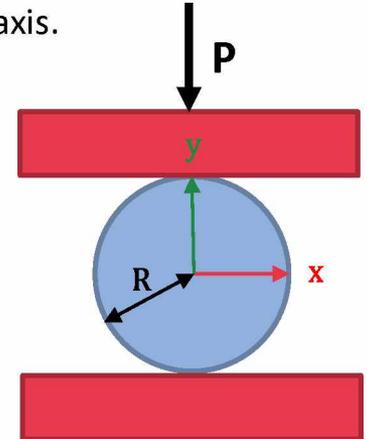
$$\sigma_x = \frac{-2P}{\pi L} \left\{ \frac{x^2(R-y)}{\beta_1^4} + \frac{x^2(R+y)}{\beta_2^4} - \frac{1}{2R} \right\} \quad (1)$$

$$\sigma_y = \frac{-2P}{\pi L} \left\{ \frac{(R-y)^3}{\beta_1^4} + \frac{(R+y)^3}{\beta_2^4} - \frac{1}{2R} \right\} \quad (2)$$

$$\sigma_{xy} = \frac{2P}{\pi L} \left\{ \frac{x(R-y)^2}{\beta_1^4} + \frac{x(R+y)^2}{\beta_2^4} \right\} \quad (3)$$

$$\beta_1^2 = (R-y)^2 + x^2$$

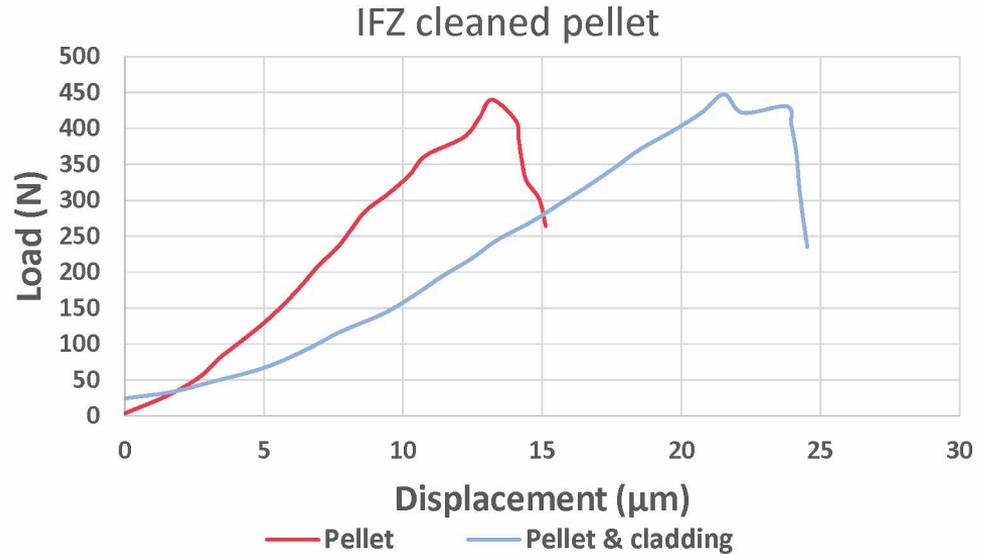
$$\beta_2^2 = (R+y)^2 + x^2$$



- Assuming that the tensile stress along the x axis is responsible for the sample failure, the tensile strength  $\sigma_f$  is obtained by substituting  $x=y=0$  into equation 1 to obtain :

$$\sigma_f = \frac{2P}{\pi DL} = \frac{P}{\pi RL}$$

### 3. Results : Tests on fragmented and pellet



	Force (N)	σ <sub>f</sub> (MPa)
<b>Pellet</b>	439	2.5
<b>Pellet &amp; cladding</b>	447	2.6

- Same fracture strength
- Brittle pellets
- Need to change the nature of IFZ for higher strength

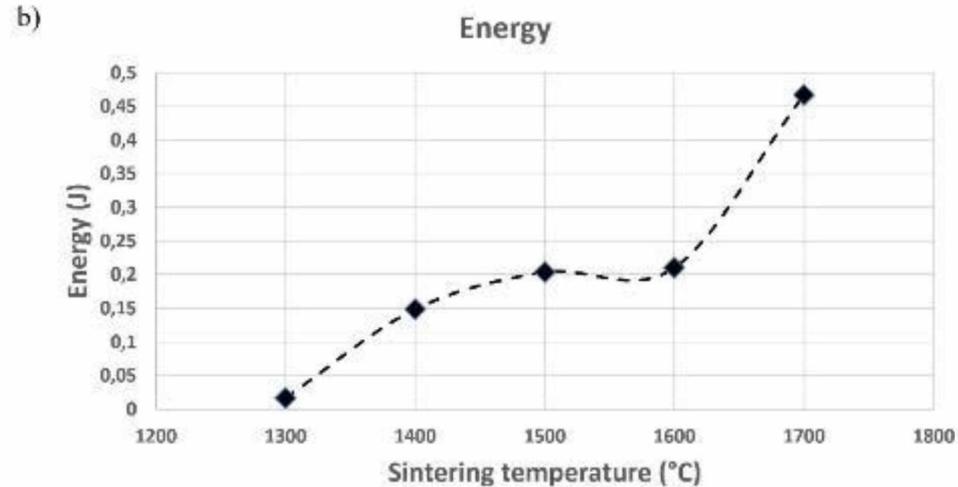
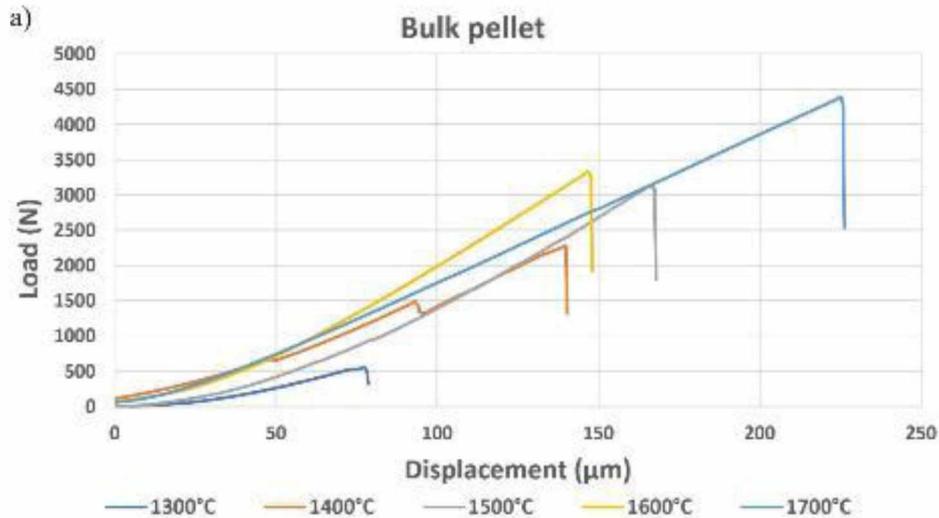
### 3. Results : New strategy of fabrication

- Following fabrication, no IFZ cleaning.
- Goal: exploiting the densification difference between the polymerized fragments and the unpolymerized IFZ.
- IFZ thickness reduced to 200  $\mu\text{m}$  for higher mechanical properties.
- Several sintering temperatures tested to ensure a good fragmentation and sufficient mechanical properties.
- Fabrication of reference bulk pellets.

IFZ



### 3. Results : Bulk pellets



Temperature ( $^{\circ}\text{C}$ )	Force (kN)	Energy (J)	$\sigma_f$ (MPa)
1300	0.6	0.02	4.3
1400	2.3	0.14	12.3
1500	3.1	0.2	34
1600	3.3	0.21	54.5
1700	4.4	0.47	107

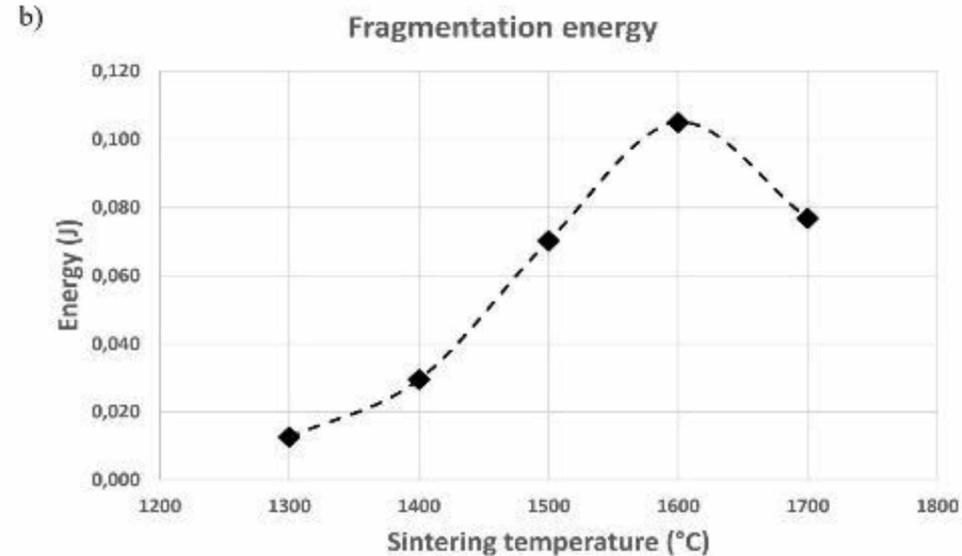
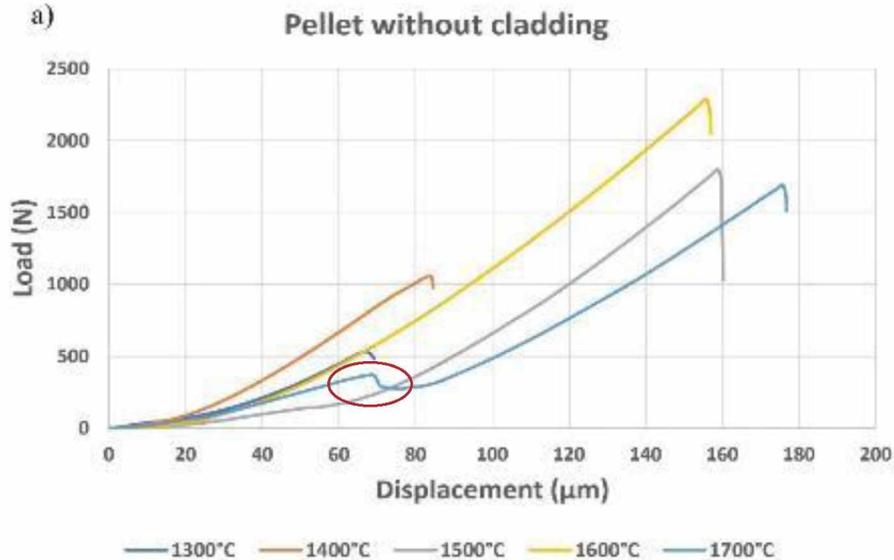
- Higher resistance with higher sintering temperature.

### 3. Results : Test on pre-fragmented and uncleaned pellets



- Fragmentation occurs mainly in the IFZ.
- IFZ-controlled fragmentation for the pellet sintered at 1700°C, as there is more individual and smaller fragments.

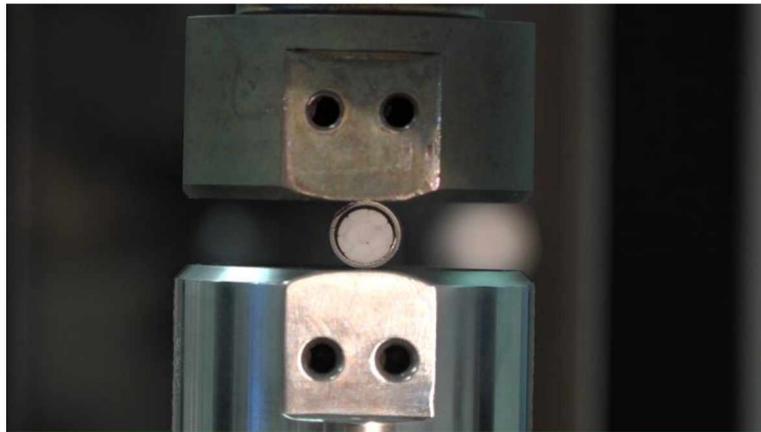
### 3. Results : Test on pre-fragmented and uncleaned pellets without cladding



Temperature ( $^{\circ}\text{C}$ )	Force (N)	Energy (J)	$\sigma_f$ (MPa)	$\sigma_f$ (MPa) Bulk
1300	527	0.01	2.9	4.3
1400	1054	0.03	6.1	12.3
1500	1797	0.07	11.2	34
1600	2287	0.11	15.2	54.5
1700	1692	0.08	10.8	107

- Same behavior as the bulk pellet.
- Higher resistance with higher sintering temperature, except for 1700°C.
- A drop at 350 N indicating a cracking which could induce a drop in the overall resistance of the pellet

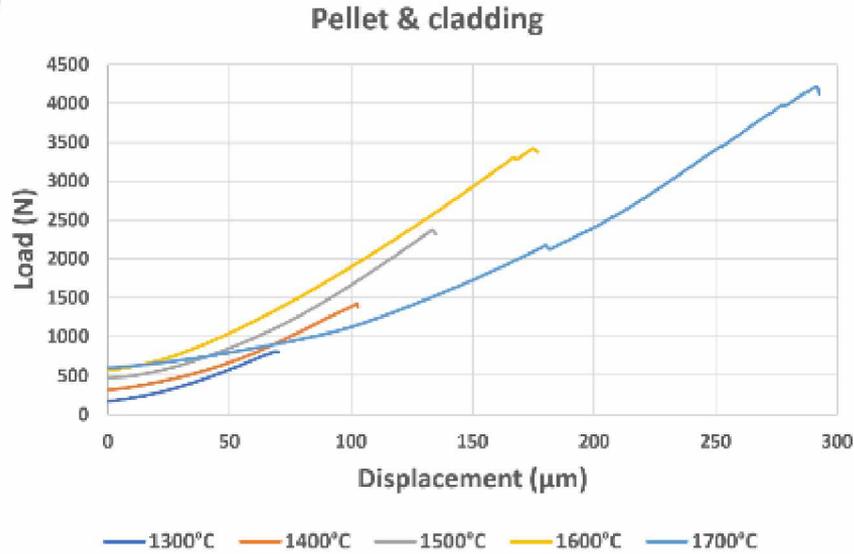
### 3. Results : Test on pre-fragmented and uncleaned pellets with cladding



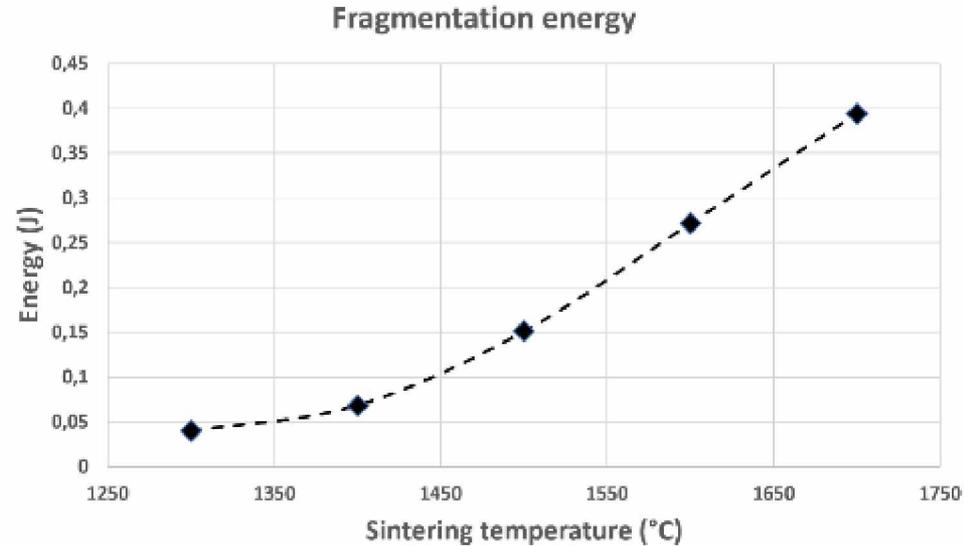
- Mostly powder for 1300 and 1400°C as the fragments are not consolidated enough.
- As before, IFZ-controlled fragmentation at 1700°C as there is more individual and smaller fragments.

### 3. Results : Test on pre-fragmented and uncleaned pellets with cladding

a)



b)

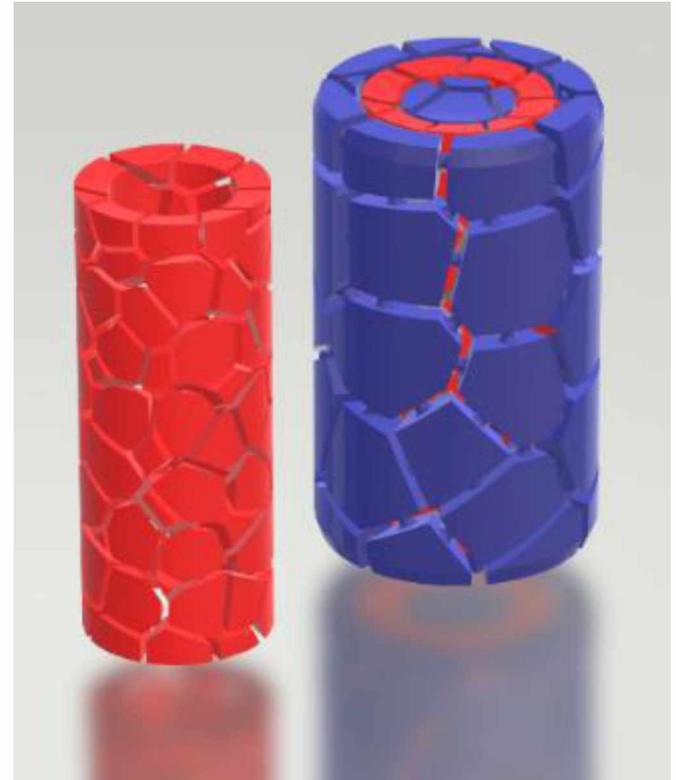


Temperature ( $^{\circ}\text{C}$ )	Force (kN)	Energy (J)	$\sigma_f$ (MPa)	$\sigma_f$ (MPa) NO cladding
1300	1.5	0.15	8.2	2.9
1400	1.4	0.07	8.4	6.1
1500	2.4	0.15	14.9	11.2
1600	3.4	0.27	22.9	15.2
1700	4.2	0.39	30.3	10.8

- Same behavior as the full pellet.
  - Higher resistance with higher sintering temperature
- Sintering at 1700°C seems to offer a good fragmentation in the IFZ, with individual fragments and high mechanical properties.

## 4. Conclusions and prospects

- Excessive embrittlement for IFZ cleaned pellet
- Uncleaned pellets still offer a good fragmentation with higher mechanical properties.
- Chosen sintering temperature: 1700°C.
- Future work:
  - Fabrication of 40 pre-fragmented pellets at 1700°C to perform a Weibull's statistics
  - Performing a semi-integral test on the pre-fragmented pellets
  - Fabrication and mechanical characterization of new pellets with different sizes of fragments
  - Towards DEM modeling to support experimental data



*Thank you for your attention*