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Comparison of two methods for assessment of the rod positioning uncertainty and consequences on the evaluation of correlation factors

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In this paper two major families of methods to deal with the assessment of the rod positioning uncertainty in a lattice are tested: a traditional one described in the *International Handbook of Evaluated Criticality Safety Benchmark Experiments* (IHECSBE) Handbook and the other one consisting in sampling the position of rods with Monte Carlo techniques (ISO Uncertainty Guidelines). They are applied on a benchmark with tight-packed lattice of UO₂ rods that is sensitive to the rod positioning as it is clearly under-moderated. It is shown that the choice of the method has a great impact on the propagated uncertainty, the traditional one leading to a significant overestimation of the overall uncertainty and can also contribute to a bias in the correlation factors that are used for assessing biases due to nuclear data using GLLSM methodologies. The paper briefly describes the tight-packed lattice experimental program performed at the Valduc Research Centre, which is at the origin of these concerns. Then it proposes a simple model on which to apply simulations of rod positioning to be performed with MORET 5 Monte Carlo code using the Prométhée tool. Results demonstrate that use of Monte Carlo methodologies provide more realistic uncertainty estimates in fuel pitch that are consistent with repeatability/reproducibility experiments. The current comparisons use light water reactor systems, which is directly relevant to some small modular reactor designs. However, accurate prediction and estimate of uncertainties in pitch for advanced reactor systems is also relevant. The application of unrealistic uncertainty analysis methods can incur larger margins in advanced reactor design, safety, and operation than are necessary.

KEYWORDS

ICSBEP, Monte Carlo sampling, positioning uncertainty, prométhée, uran

1 Introduction

For several years now, the criticality community has made efforts to provide documented critical experiments with “best-estimate” uncertainties that could be of interest for the validation of criticality codes. A project named International Criticality Safety Benchmark Evaluation Project (ICSBEP) was created in 1992 for that purpose (Briggs, Scott, and Nouri 2003). In that prospect, experiments from diverse laboratories and covering a wide range of applications were evaluated. A part of the evaluation consists of determining the chemical and geometrical uncertainties. Sometimes just a few parameters can drive the overall uncertainty. When designing experimental programs, people in charge of the design of experiments try to select moderation values as close as possible to the moderation optimum. One of the reasons is that the closer the moderation ratio is to the optimum, the lower the uncertainties in rod positioning and fewer rods are needed to reach criticality. However, in the French tight-packed-lattice experiments, LEU-COMP-THERM-071 (Leclaire 2019a), LEU-COMP-THERM-072 (Leclaire 2019b), and LEU-COMP-THERM-073 (Leclaire 2019c), the experiments have pitches smaller than required for optimal moderation, as they were designed to slightly shift the sensitivity of k_{eff} to the epithermal energy range with a view to address the economic needs of nuclear operators with a more compact storage. Therefore, the uncertainty contribution from rod positioning is greater.

In fact, when the spacing between rods corresponds to the fissile medium moderation ratio optimum, the positioning uncertainty is negligible. However, when the spacing between rods is smaller when we get further from the moderation ratio optimum, the impact is much greater. Depending on the pitch between rods, the positioning uncertainty can have a varying effect upon k_{eff} . The situation where the moderation ratio is far from the optimum ratio could be encountered in advanced reactor design concepts, including microreactors. During the design and operations, the uncertainty in the positioning of rods due to the tolerance values of grids’ holes and fuel rods is considered in the calculations. A propagation method based on MC sampling can help in determining the best estimate of the overall uncertainty and mitigating overestimation of margins supporting safety and operations.

Moreover, with the growth of advanced tools used to estimate the biases due to nuclear data such as TSUNAMI (Rearden 2004), WHISPER (Brown, Rising, and Alwin 2016), and MACSENS [Fernex], the accurate determination of correlation factors between experimental cases has become an important issue. The determination of such values is conditioned by a thorough evaluation of uncertainties, and the associated random and systematic components of each uncertainty.

To sum this up, different ways of propagating the uncertainty in terms of Δk_{eff} can be envisioned, amongst which what can be

called “traditional” ones based on ICSBEP recommendations and other ones based on Monte Carlo (MC) simulations. Depending on the method, the impact on Δk_{eff} can be completely different. The aim of this work is to compare the traditional methods with methods using MC simulations on variable sizes of lattices as proposed in the International Organization for Standardization (ISO) uncertainty guides (referred to in this document as the ISO GUM S1 procedure) (JCGM 2009) (JCGM 2008) and to compare with repeatability/reproducibility experiments allowing access to such uncertainty.

2 Description of the configuration

2.1 Tight-packed lattice pitch program

From 1998 to 1999 a series of critical experiments referred to as the tight-packed lattice experimental program was performed using Apparatus B in the Commissariat à l’Energie Atomique (CEA) Valduc Research Centre in France (Duhamel and Girault 2006). The experimental device, shown in Figure 1A, is commonly used for assembling configurations with epithermal and thermal neutron energy spectra. These experiments, designed by L’Institut de Radioprotection et de Sûreté Nucléaire (IRSN), and funded by COGEMA (also formerly AREVA NC and now Orano Cycle) and IRSN, involved UO_2 rods at a 1.05-, 1.075-, 1.1- or 1.6-cm square pitch and contributed to the validation of uranium cross sections in thermal and epithermal energy ranges. Twenty-seven critical experiments were performed, evaluated, and analyzed with different criticality software packages. The experiments were slightly sub-critical, the water level being raised until $k_{\text{eff}} = 1 - (\beta_{\text{eff}}/10)$. The water critical level was obtained by extrapolation of the inverse neutron counting rate.

The first step of the program involved lattices of 1.1-cm square pitched UO_2 rods moderated and reflected by water (documented in LEU-COMP-THERM-071). The UO_2 rods were a typical design for a pressurized-water reactor (PWR) with a ^{235}U enrichment of 4.738 wt%. The main characteristics of the fuel rods are given in Table 1 (uncertainties are indicated as 1σ). The uncertainties of the rods are mainly due to the precision of measurement devices and are therefore assumed to be 90% systematic. The UO_2 rods consisted of vertically stacked pellets contained within Zircaloy-4 cladding. The rod diameter corresponded to the industrial fuel pin diameter. The fuel stack length was adjusted to the height of the experimental tank, which was equal to 90 cm. Experimental uncertainties for the rod characteristics are also gathered in Table 1.

Sensitivity studies were performed to assess the impact on k_{eff} of various experimental uncertainties upon the configuration in accordance with the recommendations of the IHECSBE uncertainty guide (Dean 2008). The effects on k_{eff} changes were adopted as the associated components of the k_{eff} uncertainty. In order to compare different methods of rod

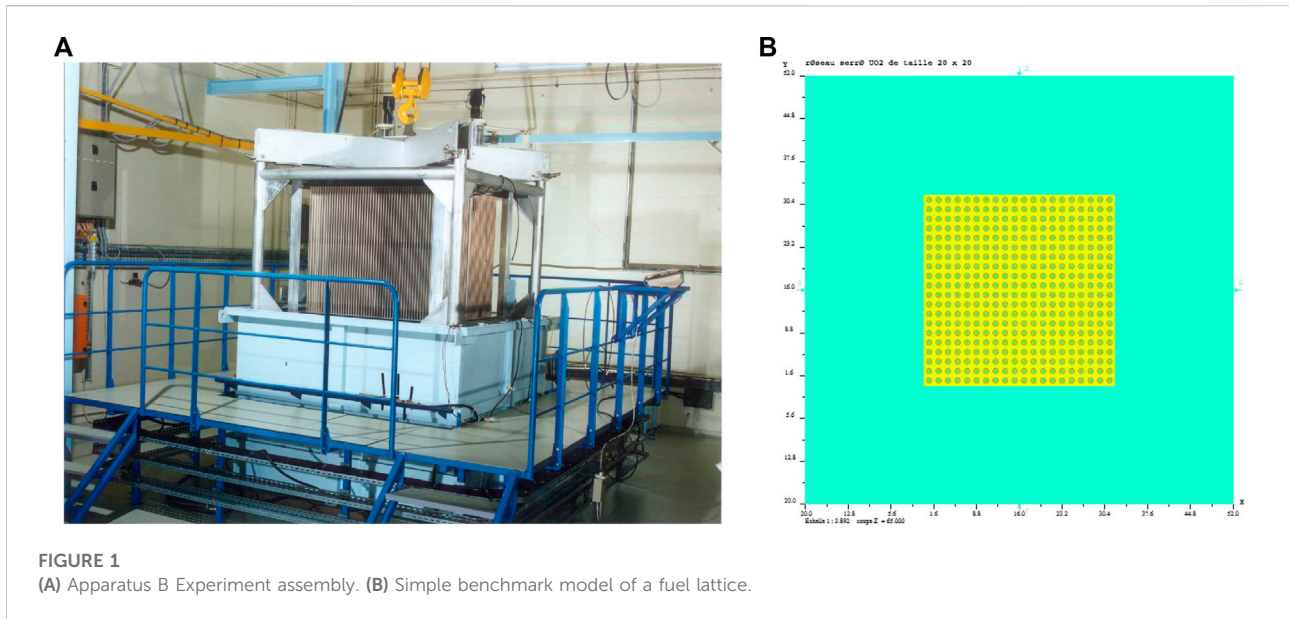


FIGURE 1
(A) Apparatus B Experiment assembly. **(B)** Simple benchmark model of a fuel lattice.

TABLE 1 Primary experiment parameters and uncertainties for LEU-COMP-THERM-071 (Leclaire 2019a).

Parameters	Value	Uncertainty
UO₂ rods		
Uranium Vector (wt%)		
²³⁴ U	0.0302	0.0005
²³⁵ U	4.7376	0.0020
²³⁶ U	0.1362	0.0005
²³⁸ U	95.0959	0.0010
Oxide impurities (ppm)	204	204
Fuel Pellet	0.78919	0.00176
Diameter (cm)		
Fuel Density (g/cm ³)	10.38	0.073
Inner Clad	0.836	0.005
Diameter (cm)		
Outer Clad	0.94924	0.00044
Diameter (cm)		
Density (g/cm ³)	10.38	0.22
Experiment Data		
Temperature (°C)	20	2
Rod Positioning (Pitch and Grid Hole Diameter) (cm)	1.1	0.023

positioning uncertainty, the uncertainties of two revisions (0 and 1) of the LEU-COMP-THERM-071 benchmark are reported in Table 2. The main components of the k_{eff} errors are shown in Table 2 for the first series of experiments along with the overall propagated uncertainty, calculated as the square root from sum of squares of its individual components. The differences between revision 0 and revision 1 are mainly associated with the fact that

random uncertainties were ignored in revision 0 and are taken into account in revision 1. Moreover, the rod position being the source of large uncertainty, its treatment has been modified using Monte Carlo sampling in revision 1, contributing to a reduction of its propagated value. It can also be seen that for cases with a small pitch the rod positioning has a non-negligible effect on the overall uncertainty.

TABLE 2 Evaluated Experimental 1 σ Uncertainties (in pcm) for LEU-COMP-THERM-071 Experiments.

Uncertainty component	Revision 0	Revision 1	Type of uncertainty
UO₂ Rods			
Isotopic Content	6	6	Systematic (precision of device)
Oxide Impurities	17	17	Systematic (tolerance level)
Pellet Diameter	2	22	Mixed (Measurement of 53 pellets + device uncertainty)
Fuel Density	Negligible	42	Mixed (Measurement of 1261 rods + precision of device)
Inner Clad Diameter	18	23	Systematic (tolerance value)
Outer Clad Diameter	1	29	Mixed (Measurement of 300 pellets and precision of device)
Experiment Data			
Temperature	7	5	Systematic (variation of temperature range)
Rod Positioning (Pitch and Grid Hole Diameter)	67	20	Mainly random (position of rod inside grid)
Total	72	66	

The bold values are the total uncertainty, which was derived from the individual component uncertainties listed above them in the table.

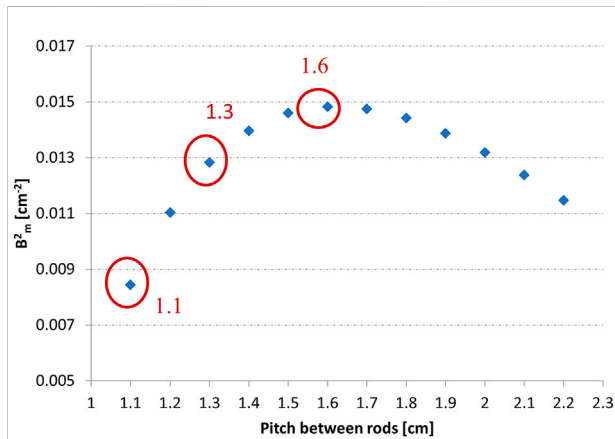


FIGURE 2 Material buckling versus pitch between rods. The pitch between rods correspond with the distance between the centers of two neighboring rods. B^2_m is the material buckling.

TABLE 3 Array dimension versus moderation ratio.

Array dimension	Pitch (cm)	V_{mod}/V_{ox}
35 × 35	1.1	1.028
25 × 25	1.3	1.823
17 × 17	1.6	2.032

2.2 Simple model

To test efficiently the different methods, it seems reasonable to define a simple benchmark, shown in Figure 1B, with which they can be tested. This benchmark is made of three different lattices of UO₂ rods having the same characteristics as the Valduc rods (see Section 2.1). The variable parameter is the pitch between rods (1.1, 1.3, and

1.6 cm). The smallest pitch corresponds to an under-moderated lattice and the largest pitch to the moderation optimum as can be seen in Figure 2, where is reported the material buckling (B^2_m) versus the pitch between rods. The moderation ratio, V_{mod}/V_{ox} , values are reported in Table 3.

In order to have a k_{eff} close to 1, the number of fuel rods is adjusted accordingly. The 1.1-cm pitch lattice comprises an array of 35 × 35 rods, the 1.3-cm lattice an array of 25 × 25 rods and the 1.6-cm pitch lattice an array of 17 × 17 rods. It is to be noticed that the moderation optimum corresponds to a pitch of 1.6 cm between rods for a 4.738 wt% ²³⁵U enrichment. The rod plugs were not considered in the model; only the fissile column surrounded by its cladding was retained. The height of rods was then set equal to 89.765 cm. The lattices were centered in a parallelepiped box, containing water, of 130-cm height and side dimensions corresponding to the lattice size plus 20 cm.

3 Calculation tools

Calculations were performed using the MORET 5 Monte Carlo code (Cochet, et al., 2015) and the computing environment Prométhée (Richet et al., 2007).

3.1 The MORET 5 monte carlo code

Calculations were performed using the MORET 5 continuous energy Monte Carlo code. It is a 3D MC code for neutron transport developed at IRSN for criticality safety assessments. It employs continuous energy cross sections derived from JEFF-3.1 evaluated nuclear data files (Koning et al., 2006). Typically, each calculation k_{eff} was run to achieve a precision of ±0.00010 Δk_{eff} (±10 pcm).

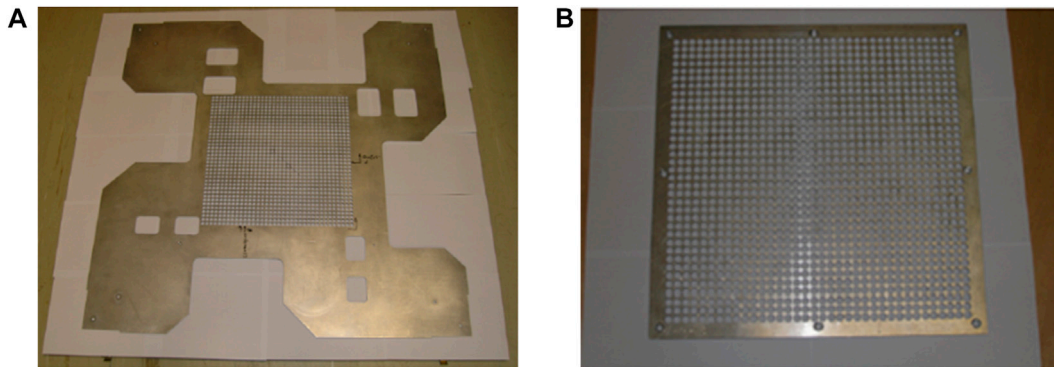


FIGURE 3
Upper (A) and lower (B) grids of LEU-COMP-THERM-071 experiments.

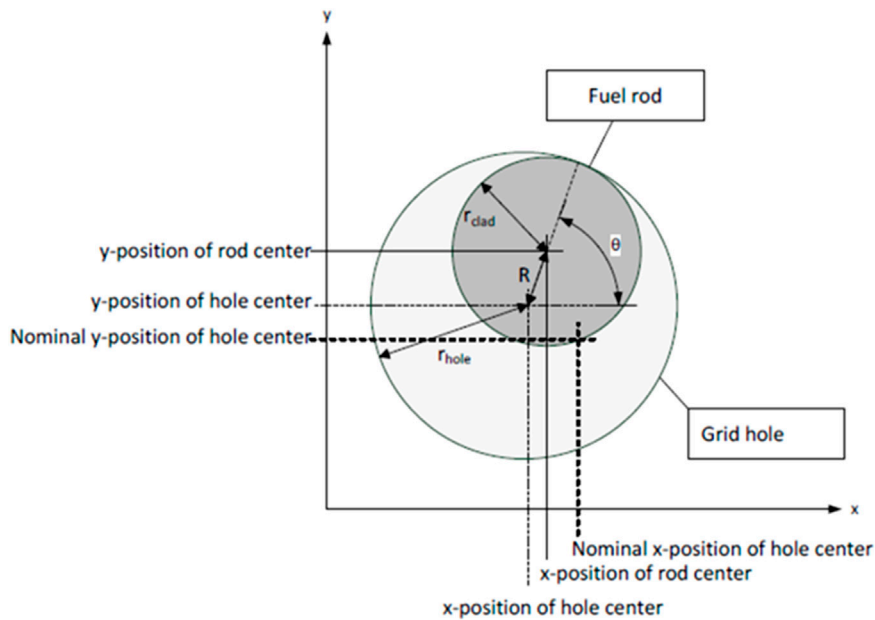


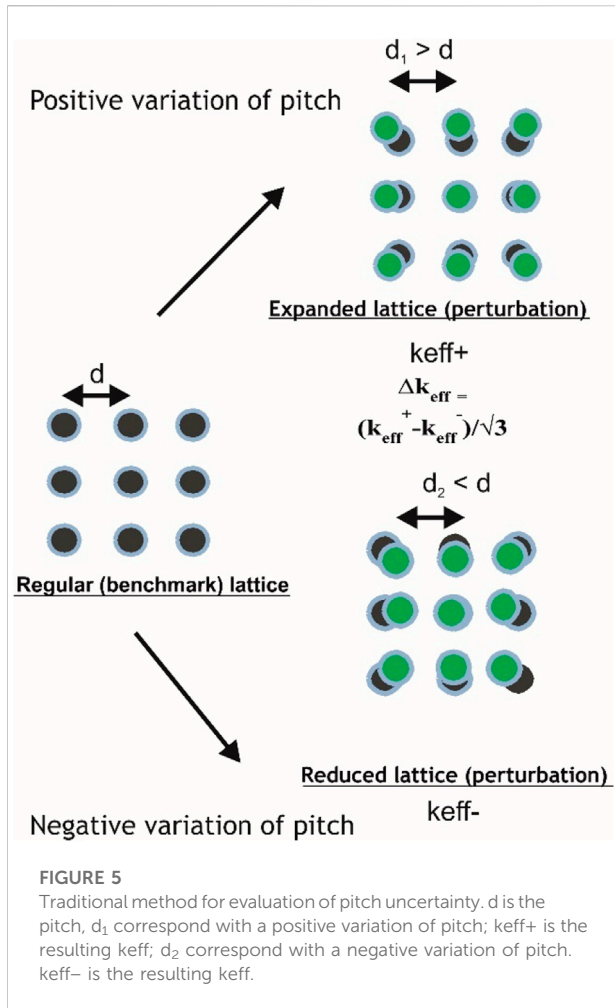
FIGURE 4
Rod location uncertainty: Detail of a rod in its grid hole.

3.2 Description of prométhée tool

Prométhée is a grid computing environment designed to provide engineering methodologies relevant for any available code. The Prométhée system is composed of a Graphical User Interface (GUI) designed to provide ergonomics features for a computing software input data engineering algorithms (for instance uncertainties propagation methods). Then, calculations are remotely performed on servers. The parameterization of rods' location in the lattice was performed using Prométhée.

4 Description of the different methods to assess the rod positioning uncertainty

At first look, the origin of the rod positioning uncertainty is mainly linked with the presence of two grids (both upper (A) and lower (B) are shown in Figure 3) drilled with holes with a slightly higher diameter; the spacing between rods is conditioned by the grid plate holes. These two grids ensure the mechanical rigidity of the lattice.



As illustrated in Figure 4, The uncertainty of rods' positioning is composed of:

- Hole position uncertainty due to error in adjustment of the grid hole piercing device: ± 0.001 cm manufacturing tolerance;
- The uncertainty of the outer diameter of the rod cladding: ± 0.00044 cm (1σ);
- The uncertainty of the grid holes' diameter: ± 0.0085 cm (1σ); and
- The uncertainty of the gap between the rod and the edge of the grid hole (tolerance of ± 0.0407 cm): corresponds to a 1σ -uncertainty of ± 0.023 cm.

All in all, a total 1σ -uncertainty of ± 0.033 cm is obtained. The different components of the spacing uncertainty are converted in an increase or decrease of the distance between rods.

4.1 Traditional method

The way the uncertainty in rod positioning is propagated varies from one evaluator to another and from one calculation code to another. One of the examples given to evaluators in the IHECSBE consists of varying the spacing between all rods from plus or minus the uncertainty of the gap. The reactivity difference between these two calculations divided by two times the square-root of three (representing the correction from a two-sided bounding uncertainty with uniform probability distribution to a standard 1σ Gaussian uncertainty) determines the effective uncertainty in k_{eff} . The resultant value is then divided by square root of total number of rods. Historically, this method derived from the use of cell codes to evaluate this type of uncertainty.

As shown in Figure 5, this method was applied by shifting the rods nearer or further away from each other. The spacing between two neighboring rods was assumed to be the same throughout the lattice. Thus, the moderation ratio was varied by the same amount for all the lattice rods. For each lattice size, 2 MC calculations were performed: one, increasing the spacing between rods of a given quantity and another decreasing the spacing by the same amount. The variation was chosen in order to remain within the linearity domain of k_{eff} variations yet still large enough not to be influenced by the MC standard deviation of the calculation.

Then, the obtained k_{eff} value was scaled to 1σ and, divided by square-root of the number of rods. This factor was derived in Eq. 1:

$$\sigma^2(\Delta k_{eff}) = \sum_i \sigma^2(\Delta k_{rod,i}), \tag{1}$$

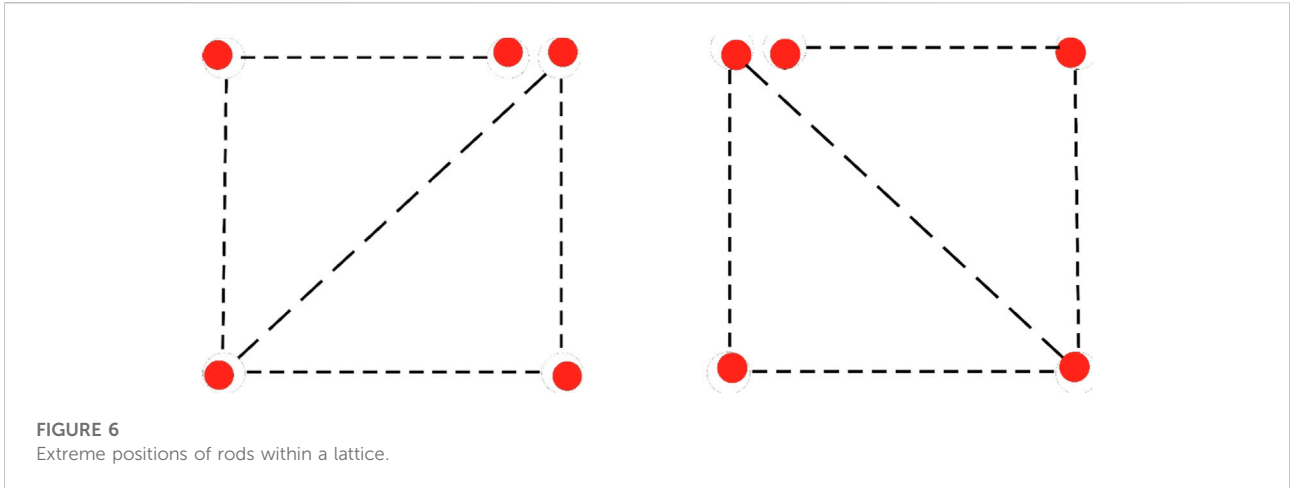
which assimilated the overall uncertainty to the sum of each rod uncertainty. When assuming that the independent contribution of each rod to the overall uncertainty is the same, the formula can be written as shown in Eq. 2:

$$\sigma^2(\Delta k_{lattice}) = N \times \sigma^2(\Delta k_{rod}). \tag{2}$$

The last assumption consists in saying that the variance of the lattice is the total variance divided by N as described in Eq. 3:

$$\sigma^2(\Delta k_{lattice}) = \frac{\sigma^2(\Delta k_{eff})}{N}. \tag{3}$$

For large lattices of rods, assuming that the contribution of the uncertainty of each rod is the same leads to a biased estimation of the uncertainty. A calculation separating the assembly in two zones (internal and peripheral) and assessing separately uncertainties on these two zones should ideally be considered. However, it will not be investigated in this paper.

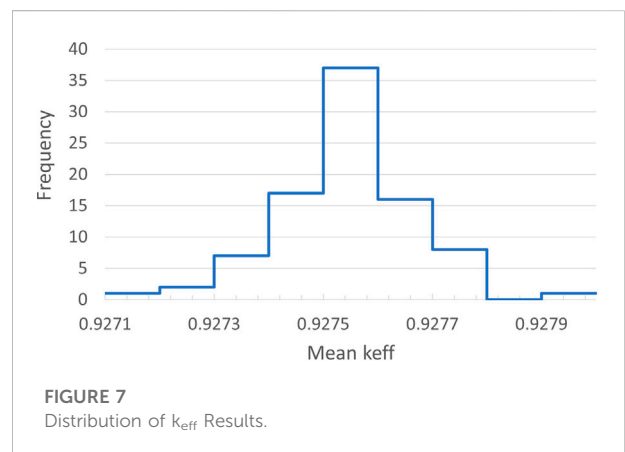


4.2 Refined traditional method

The “refined traditional” method is a variant of the basic traditional method. The only difference is that the Δk_{eff} is divided by the square-root of an additional factor (k_R) to account for the fact that the position of rods is constrained within a grid and that there is a compensation effect for the simultaneous variation of pitch between all rods. This factor (Ivanova, Ivanov, and Bianchi 2014) is called the peak-to-average ratio and is typically constrained between the values of 1.3 and 1.5.

4.3 Extreme lattice bounds

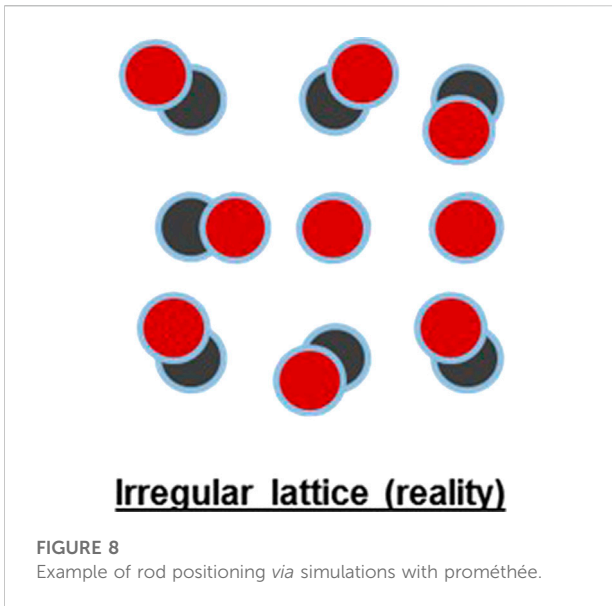
Another variant of traditional methods leans upon the fact that the rod position is constrained within the grids. The rods cannot move outside their grid holes. As a consequence, it is impossible to impose the maximum shift to all the rods at the same time. The average rod position is constrained between two extreme positions that are demonstrated in Figure 6. For that reason, the method could be called “extreme lattice bounds.” The mean variation of rod position is equal to the difference of width between these two lattices divided by the square-root of the total number of rods in the lattice. In fact, in the X direction for instance, only the distance separating the two last rows of rods at the periphery is modified. The modification is equal to the gap between the rod and the grid hole multiplied by $\sqrt{2}$. As a consequence, the average rod position shift is the gap $\times \sqrt{2}/\sqrt{N}$ with N being the total number of rods in the lattice. When propagated in terms of Δk_{eff} , this variation leads to results comparable to traditional methods but slightly lower.



4.4 Monte Carlo sampling with MORET 5/ Prométhée

Two kinds of MC simulations were tested during this work. The first one uses the MORET 5 code combined with the Prométhée workbench to do the MC sampling. A first step consisted in comparing the traditional method varying the pitch value according with a chosen distribution law. The variation was then propagated in terms of Δk_{eff} for 100 different rod positioning maps corresponding to 100 different simulations. Then, the distribution of k_{eff} was observed.

A second step consisted in comparing the traditional method with a simulation on the position of rod according to ISO GUM S1 standard procedure. Instead of increasing artificially the distance between rods of the same quantity, the position of



rods in their holes was sampled independently 100 times (this number was chosen arbitrarily but was found sufficient to have a Gaussian distribution, as shown in Figure 7, which was confirmed by the value of the bootstrap) for the 35 × 35 array and propagated in terms of Δk_{eff} using the ISO GUM S1 standard procedure, which corresponded to a more realistic approach. For this method, the position of each rod was chosen independently

from its neighbors. The Δk_{eff} was observed and its statistical parameters (mean and variance) were estimated (Figure 8).

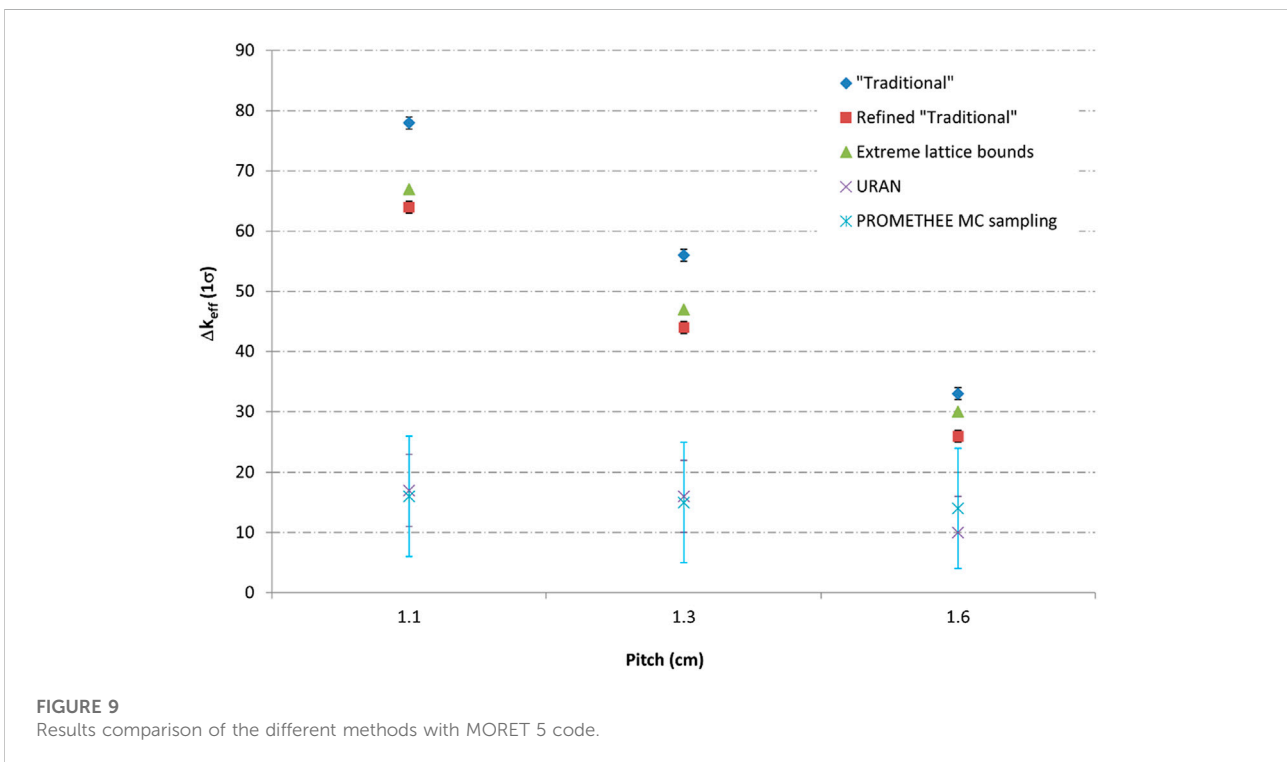
4.4.1 Sampling of rod positioning

In this section, the position of rods varies independently from the position of neighboring rods (Figure 9), which is more realistic than the use of traditional methods. The position of rods is constrained since they are held by two grids (lower and upper). As explained at the beginning of section IV, the rods can move within their grid holes. Their uncertain position pertains to the external diameter of claddings, the precision of the piercing of grid holes, and to the gap existing between the rods and the grid holes. In fact, with the increase of water level during a critical approach, the rods can move inside their grid holes and their respective positions can be correlated. The overall positioning uncertainty was chosen to follow a uniform distribution. Each rod position was supposed to be completely uncorrelated from that of its neighbors. Thus, the distance between rods was not the same throughout the lattice. The parameterized variable was the position of rods. For each lattice, the input listings were automatically generated with Prométhée tool.

The rods position shifts are given by Eqs 4, 5 in the X and Y lattice directions, respectively. The maximum shift was estimated as being equal to $2 \times .0439$ cm between two neighboring rods.

$$\Delta X = 0.0439 \times r_1^{\frac{1}{2}} \times \cosine(2 \times \pi \times t_1) \quad (4)$$

$$\Delta Y = 0.0439 \times r_1^{\frac{1}{2}} \times sine(2 \times \pi \times t_1) \quad (5)$$



The variables r_1 and t_1 were chosen randomly according with an equiprobable distribution law. This assumption is over-predicting the uncertainty propagation in comparison with a triangular or Gaussian distribution law. By default, this option was retained. The size of the modeled lattice is chosen accordingly with the pitch between rods as defined in section 2.2.

For each lattice, a batch of 100 calculations corresponding to 100 different values of (r_1, t_1) , with a MC precision of $\pm 0.00010 \Delta k$, was launched on 100 different computing nodes *via* the Prométhée plugin. A fixed number of neutrons per lattice (10,000) was chosen. It has been checked that this number had hardly any impact upon k_{eff} . It should be noticed that the observed variance is the sum of both code k_{eff} estimate variance (MC codes) and studied rod positioning effect variance. These two random variables being independent, the rod variance is estimated as the difference of observed variance and code variance.

Moreover, the value is known with a small standard deviation (<3 pcm) (Davison, Hinkley, and Schechtman 1986) due to the sample size of 100. The obtained value is far lower than the one obtained using the traditional method. Even if the comparison has been done on a simple benchmark model, the ratio obtained between the uncertainty given by the traditional method and that obtained from the ISO GUM S1 simulations can be transmitted to a configuration close to that model. This procedure applies for the tight-packed lattice program. A rod positioning uncertainty of about 70 pcm is obtained with the traditional method for a 4.738 wt% ^{235}U enrichment and a 35×35 rods lattice. For the same rods at the same moderation ratio, the “best estimate” value of the rod uncertainty can be assessed as being closer to 20 pcm.

4.4.2 Limits of the method

It should be stressed that the validity of the method leans mainly on the MC sampling. It is conditioned by the number of neutrons per batch and per volume in the geometry. A comparison with a deterministic method would be needed to definitively validate it without potential deviation due to MC sampling of neutrons (including MC Markov chain initial transient).

4.5 Monte Carlo simulations with URAN card in MCNP

Another approach consists in using the Monte Carlo N-Particle (MCNP) code, version 6, with the URAN card (Goorley et al., 2013). This card allows selecting universes to randomly translate the geometry inside a lattice cell. The Universe corresponding to the main cell of the lattice is then selected and the rods are randomly shifted within its cell. The same .0439 cm variation is defined as for the previous method involving random sampling. The position of rods is shifted of the

following quantities in the X and Y directions according to Eqs 6, 7, respectively.

$$\Delta X = (2t_1 - 1) \times \delta_1 \quad (6)$$

$$\Delta Y = (2t_2 - 1) \times \delta_2 \quad (7)$$

Here, t_1 and t_2 are random variables comprised between 0 and 1, and δ_1 and δ_2 are user-defined variations.

5 Results

5.1 Traditional and refined traditional methods

The MORET 5 results for the three lattice pitches of the benchmark are given in Table 4. The JEFF-3.1 evaluation is used for the nuclear data library. Quite similar results are obtained with the two traditional methods, the results of the refined traditional being a little lower. Moreover, for a same pitch variation, the propagated 1σ uncertainty is greater for the lowest pitch, which was predictable since a tight-packed lattice of rods is more sensitive to a pitch variation than a lattice at the moderation optimum.

5.2 Results of Monte Carlo sampling and URAN

The calculations were performed for the two methods (MC sampling with MORET 5/Prométhée and URAN card with MCNP) for a rod positioning uncertainty of ± 0.04 cm. The results are reported in Table 4. It can be shown that there is no great influence of the pitch value and that the two methods are quite consistent since there is no significant difference between the results.

5.3 Comparison of the different methods

For the three pitches of the benchmark and a shift of the position of rods corresponding to the 1σ uncertainty of rod position, calculations were performed with the continuous energy Monte Carlo MORET 5 code and the various methods presented beforehand. These results are reported in Figure 9. It can be shown that the traditional methods lead to higher Δk_{eff} values than the methods based on MC sampling or the URAN card in MCNP6. The reduced uncertainty using the URAN card with MCNP is consistent with similar comparison studies performed for the Neutron Radiography (NRAD) reactor (Bess, Maddock, and Marshall 2014). The discrepancy is more important for smaller pitches. In fact, at moderation optimum, the MC sampling methodology is not necessary since quite

TABLE 4 Comparison of Methods for Pitch 1σ Uncertainty (in pcm).

Pitch uncertainty (cm)	Traditional	Refined	Extreme lattice bounds	Monte Carlo sampling	URAN
Pitch = 1.1 cm					
.02	38	31	67	17	16
.04	78	64			
.08	158	129			
Pitch = 1.3 cm					
.02	28	22	47	16	15
.04	56	44			
.08	112	91			
Pitch = 1.6 cm					
.02	16	13	30	10	14
.04	33	26			
.08	74	53			

consistent results are obtained. This is not the case for tight-packed lattices of rods, however. Moreover, it should be pointed out that the results obtained with MC sampling and those using the URAN card in MCNP6 are perfectly consistent. The question now is to know which method better predicts the uncertainty.

5.4 Comparison with experimental results

A way to have access to this information is to make comparisons with experimental results. Repeatability/reproducibility experiments can allow such comparison. This was done for another proprietary program called MIRTE (Matériaux en Interaction et Réflexion Toutes Epaisseurs) (Leclaire et al., 2014) whose aim was the validation of the calculation of structural materials in thermal energy spectrum. This program involved the same UO_2 rods, with a 1.6-cm square pitch (moderation optimum). The reproducibly experiment consisted in draining the water level from the tank, unloading the baskets containing the rod lattices, shake them, reload them and then perform a new critical approach. Such experiments addressed different uncertainties amongst them such as the critical height uncertainty and the rod position uncertainty. The critical level difference observed between the two experiments, when propagated in terms of Δk_{eff} , corresponded to an insignificant reactivity worth (less than 20 pcm). This value was clearly lower than what was highlighted using traditional methods. It demonstrates that traditional methods are clearly overestimating rod positioning uncertainty. Moreover, the same order of magnitude was obtained as with the MC sampling method. As a result, the results obtained with the MC sampling method or with the URAN card of MCNP 6 are not without experimental validation. One can be confident in the results they provide.

6 Consequences of correlation factors

6.1 Definition of correlation factors

Correlation factors between experiments or between cases of an experimental series are key values for the determination of biases due to nuclear data. For many years now, various tools such as TSURFER for the SCALE 6 package (Wieselquist, Lefebvre, and Jessee 2020), WHISPER for MCNP, and MACSENS (Fernex and Leclaire, 2022) for the CRISTAL package (Gomit et al., 2015) have implemented (or are implementing for MORET) a sensitivity on k_{eff} capability and the Generalized Linear Least Squares Methodology (GLLSM) to evaluate biases due to nuclear data (Broadhead et al., 1999). To correctly assess the bias, one needs to know the correlation between experiments (or cases). These values strongly influence the result of the adjustment procedure and therefore the bias. Very accurate-value correlation factors are needed. And for that, a thorough evaluation of uncertainties is required. For each parameter source of uncertainty, it is necessary to know the random and systematic components of the uncertainty to clearly demonstrate the shared uncertainty between cases. Eqs 8–11 show how these factors are calculated.

6.2 Calculation of correlation factors

Establishment of correlations between the uncertainties of a pair of benchmark experiments (called experimental correlations hereafter) is not a trivial task. If an uncertainty component is wholly or partially common for a pair of experiments, the problem is reduced to estimating the component correlation coefficient related to that specific component of the uncertainty.

TABLE 5 Comparison of 1σ Uncertainties (in pcm) for LEU-COMP-THERM-071 using Two Scenarios.

Uncertainty component	Traditional (case 1)	Traditional (case 4)	MC sampling (case 1)
UO₂ rods			
Isotopic Content	6	6	6
Oxide Impurities	17	17	17
Pellet Diameter	22	22	22
Fuel Density	42	42	42
Inner Clad Diameter	23	18	23
Outer Clad Diameter	29	27	29
Experiment Data			
Temperature	5	7	5
Rod Positioning (Pitch and Grid Hole Diameter)	58	67	20
Total	86	90	66

The bold values are the total uncertainty, which was derived from the individual component uncertainties listed above them in the table.

$$r_{m,n}^i = \frac{\delta_m^{i(s)} \delta_n^{i(s)}}{\delta_m^i \delta_n^i} \tag{8}$$

$$[\delta_n^i]^2 = [\delta_n^{i(s)}]^2 + [\delta_n^{i(r)}]^2 \tag{9}$$

$$[\delta_n]^2 = \sum_i [\delta_n^i]^2 \tag{10}$$

$$r_{m,n} = \frac{1}{\delta_m \delta_n} \sum_i \delta_m^i \delta_n^i r_{m,n}^i \tag{11}$$

Where, δ_n is the total uncertainty of the nth experiment; δ_n^i is the *i*th component of the total uncertainty of the nth experiment; $\delta_n^{i(s)}$ and $\delta_n^{i(r)}$ are the systematic, i.e., common, and random parts of the *i*th component for nth experiment's total uncertainty, respectively; $r_{m,n}^i$ is the component correlation coefficient for the *i*th uncertainty component for experiments m and n; and the coefficient $r_{m,n}$ varies between 0.0 and 1.0, i.e., between non-correlated and fully correlated systems, respectively.

In order to demonstrate that correlation factors between experiments are dependent upon the evaluation of experimental uncertainties, an application case is chosen. The tight-packed lattice program, LEU-COMP-THERM-071, is chosen for that aim. We will show how the evaluation of the rod positioning uncertainty can influence the value of correlation factors. Two cases are selected: one with a 1.1-cm square pitch (case 1 of Table 5) and the other with a 1.075-cm square pitch (case 4 of Table 5). The detail of experimental uncertainties is provided with in Table 5. Two scenarios are retained concerning the evaluation of the rod positioning uncertainty: traditional method or Monte Carlo sampling. Cross cut views of the two model lattices are reported in Figure 10.

The rod positioning uncertainty appears to be driving the overall uncertainty. The correlation factors were calculated assuming that the uncertainties pertaining to all parameters

are 100% systematic (in fact, the random part of the uncertainty is negligible when compared to the systematic part), except for the rod positioning uncertainty where it is supposed to be random for both scenarios. Even if there is some systematic uncertainty on the grid hole position due to the manufacturing procedure, the rod positioning uncertainty is mainly random. Indeed, the rods are inserted manually in the grids' holes and lean on their bottom plug. Once positioned in the grids' holes, they can move randomly within the holes during the critical approach due to the increase of the water level or can even move due to vibrations. Moreover, the positions of rods being not marked in the lattice, from one case to another, the position is resampled, and the positioning uncertainty is random. When looking now at the correlation matrix below, one can see that the correlation factor is strongly dependent on the chosen scenario, for tight-packed lattices of rods. It would not be the case for lattices of rods at moderation optimum.

$$\begin{matrix} \text{Traditional} & \text{MC} \\ \begin{pmatrix} 1 & 0.449 \\ 0.449 & 1 \end{pmatrix} & \begin{pmatrix} \text{Sampling} \\ 1 & 0.859 \\ 0.859 & 1 \end{pmatrix} \end{matrix}$$

6.3 Discussion

In this section a first attempt to understand the difference between the traditional methods and the ones using MC simulations (ISO GUM S1) is provided. It is to be noted that it is implicitly assumed while using the traditional methods that the rods are non-correlated in the contribution to overall k_{eff} . The traditional methods make the assumption that each rod contributes independently from its neighbors to the overall k_{eff} . However, the factor k_R (peak to average ratio) is

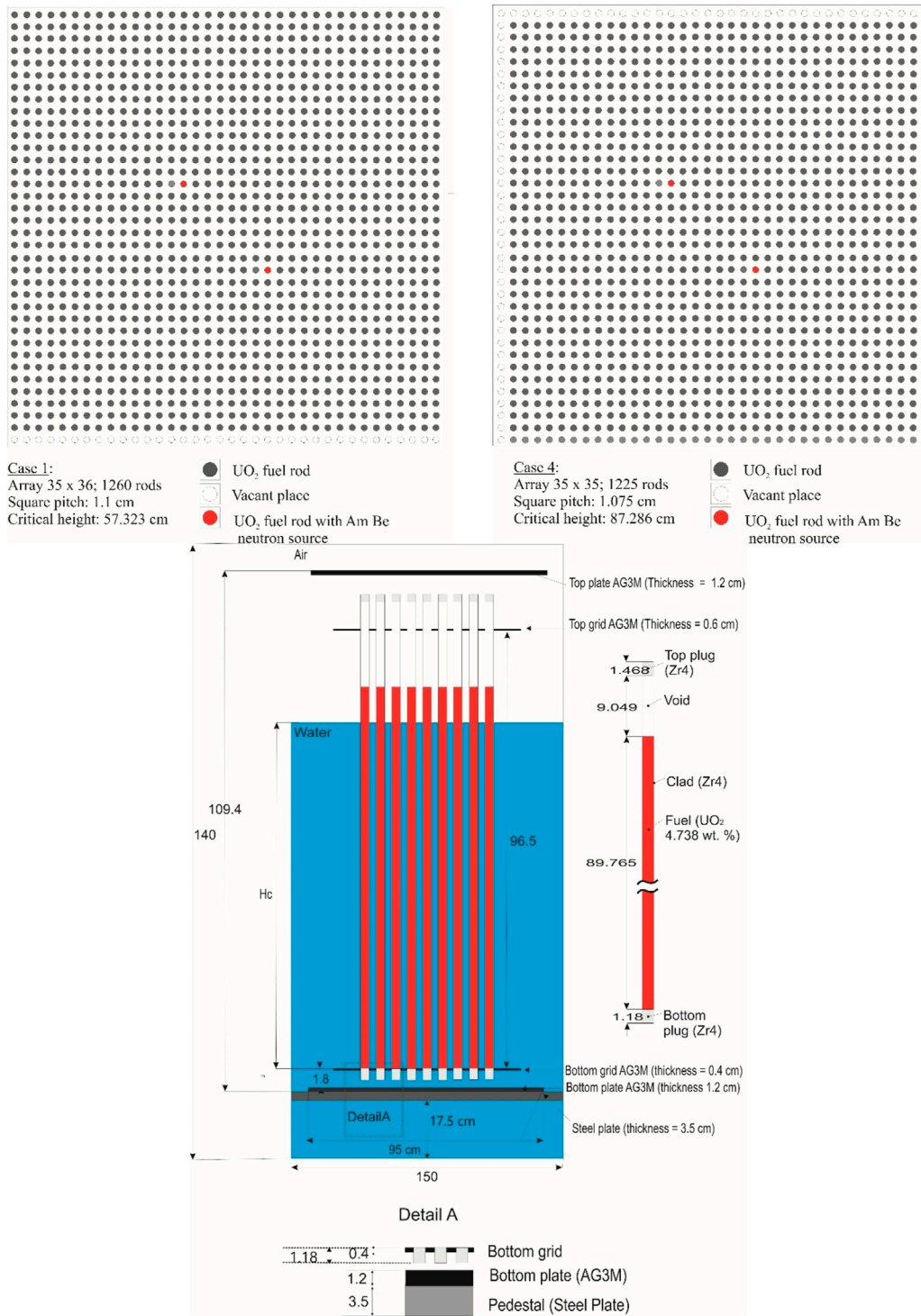


FIGURE 10
 Horizontal and vertical cross-cut views of rod lattices (LEU-COMP-THERM-071).

introduced to compensate for that by taking the correlations into account. This factor is purely empirical and depends on the rod lattice size and moderation ratio. In fact, the position of rods is

correlated since it is constrained by the presence of grids maintaining them. With the mean free path of neutrons being around 1–2 cm in a thermal spectrum, the neutrons produced in

each rod interact with at least two neighbors. Consequently, some covariance terms should contribute negatively to the uncertainty propagation. This is what is observed when doing calculations using MC sampling.

7 Consequences on criticality safety, reactor physics, and advanced reactor systems

It can be easily concluded from previous sections that the choice of the rod location uncertainty propagation methodology can have a significant impact on the overall uncertainty, especially when the fuel is under-moderated, as it is the case for LEU-COMP-THERM-071. The objective for a good assessment of calculation bias and uncertainty is not necessarily to overestimate this quantity. In criticality-safety assessment, the uncertainty in the positioning of rods due to the tolerance values of grids' holes and fuel rods is taken into account in the calculations. The same problematic applies on reactor physics design and operations. A propagation method based on MC sampling can help in determining the best estimate of the overall uncertainty, avoiding overestimation of the uncertainty with the traditional method which has historically been used.

Direct applicability of this work applies towards some of the light water small modular reactor and microreactor concepts such as the ACP100 (Danrong et al., 2021), Nuward (OECD, 2021) and Nuscale designs (Weber and Mullin 2020). As the quantity and diversity of these types of reactors expands, questions remain in not just how the uncertainties in pitch will impact reactor physics performance, but also in other core performance parameters including desired uses beyond power generation such as process heat generation for desalination, hydrogen production, or other industrial processes (IAEA 2017).

Overprediction of pitch uncertainties in advanced reactor design could lead to larger than necessary margins required for safety and operations. A simple means to understand this potential impact is to relook at the conversion of the NRAD reactor from highly enriched to low-enriched fuel (Bess, Maddock, and Marshall 2014). The initial critical mass necessary for the converted core was physically greater than computationally predicted, resulting in post-conversion accommodations to incorporate additional fuel rods into a restricted design space to enable the reactor to achieve and maintain at-power operations. While control rod worth and coefficient measurements were not significantly different from their estimates, the available core excess reactivity for operations was much less than the maximum allowed within the safety limits of the technical specifications, and nearly insufficient to enable necessary reactor operations. Uncertainties in the experiment were evaluated, including those for pitch, to estimate the impact

upon the bias between computational models and the freshly refueled reactor. Should significantly large uncertainties have been included in the design due to pitch, or any other parameter, the margins between operations and safety would have been even more significantly discrepant, possibly to the point of reactor inoperability.

Therefore, an improved approach is also of interest for advanced reactor designs such as pebble bed reactors using tri-isotropic (TRISO) fuel or other high-temperature gas-cooled reactors (HTGRs), for which the fuel-to-moderator ratio and fuel-to-fuel pitches are random; a sampling MC methodology would help evaluating the uncertainty pertaining to the fuel location. The traditional approach to column and channel pitch in prismatic HTGRs could be on the order of 0.1 % Δk_{eff} (Bess and Fujimoto 2010). While this uncertainty could be minor compared to some more significant uncertainties such as graphite and fuel properties, as manufacturing processes are improved, the approach towards treatment of geometric uncertainties becomes more prominent. However, implementation of a MC sampling methodology for TRISO particle packing in pebbles contributes insignificantly to the overall uncertainty, as expected (Çolak and Seker 2005) (Bess and Dolphin 2013). Similar expectations would apply towards fluoride salt-cooled high-temperature reactor (FHR) designs (Qualls, et al., 2017).

In fast reactor systems, significant contributors to changes in pitch can be seen in thermal expansion or bowing effects (Lum, 2018). Random rod displacement effects are mitigated and negligible if the core assemblies are suitably constrained; however, thermal expansion of grid plates and assemblies further add to the complexity in the evaluation of core neutron leakage and reactivity effects (Pope and Lum 2021). In liquid fuel systems, such as a molten salt reactor (MSR) the impact on pitch could derive from uncertainties in placement of moderator channels and blocks, if used, which can also be more suitably addressed using MC evaluative techniques (Shen, 2019), and should be further investigated as a component of evaluating technological gaps and safety requirements supporting MSR design and deployment (Forsberg 2006) (Elsheikh 2013).

A key aspect in regulation and operation of advanced nuclear reactors will require those designing and deploying the reactors to demonstrate to those regulating the operation and safety of these reactors that all aspects of systems will perform as expected. The impact of uncertainties in rod positioning is only one component of many that will need to be properly understood to satisfy regulatory requirements prior to advanced reactor deployment and operations. Ultimately, the uncertainties addressed in this paper might improve assessment of modular transportation of microreactors or fuel and their ultimate disposal; understanding biases and associated uncertainties when utilizing various methodologies and codes is imperative (Tardy, 2019).

8 Conclusion

The impact of rod positioning has been tested with various methods: the traditional one recommended historically by the ICSBEP working group, modifications to the traditional method, MC sampling using the MORET 5 code and the Prométhée computing environment, and the MCNP6 code with the URAN card to simulate the uncertain position of rods inside their grids. These methods have been applied on a benchmark involving three critical lattices of Valduc UO₂ rods with various pitches (1.1-cm, 1.3-cm or 1.6-cm square pitch) corresponding to different moderation ratios. It has been shown that the traditional methods commonly used by benchmark evaluators does not underestimate the contribution of the rod positioning uncertainty, as it was originally thought. On the contrary, for tight-packed lattices of rods (pitch 1.1 cm), a noticeable positive discrepancy with MC simulations (ISO GUM S1) is highlighted. Moreover, with a good consistency between MC sampling with MORET 5/Prométhée and MCNP 6/URAN being obtained, one can be quite confident in the result. To better estimate such a small effect, it would be necessary to perform calculations with a deterministic code.

At last, the validity of MC sampling calculations is ensured by the comparison with experimental results. Indeed, repeatability/reproducibility experiments were performed in the framework of the MIRTE (Matériaux en Interaction et Réflexion Toutes Epaisseurs) program involving similar rods in a 1.6-cm square-pitched lattice. It can be shown that the uncertain position of rods in their baskets leads to a Δk_{eff} less than ± 0.00020 , which is in accordance with the results obtained *via* MC sampling with MORET 5/Prométhée or MCNP6/URAN. Monte Carlo sampling techniques show improvement in better prediction of actual uncertainties in light water reactor systems, which is directly applicable to many small modular reactor concepts in development. However, the application of such methodologies can apply towards advanced reactor design concepts, including microreactors, to mitigate overestimation of margins supporting safety and operations.

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Data availability statement

The raw data supporting the conclusion of this article will be made available by the authors, without undue reservation.

Author contributions

NL is the main author of the paper. JB added sections to highlight the interest of such methodology for advanced reactor and complemented the list references.

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Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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Nomenclature

Acronyms

CEA Commissariat à l'Énergie Atomique

FHR Fluoride salt-cooled High-temperature Reactor

GLLSM Generalized Linear Least Squares Methodology

GUI Graphical User Interface

HTGR High-Temperature Gas-cooled Reactor

ICSBEP International Criticality Safety Benchmark Evaluation Project

IHECSBE *International Handbook of Evaluated Criticality Safety Benchmark Experiments*

IRSN L'Institut de Radioprotection et de Sécurité Nucléaire

ISO International Organization for Standardization

JFA JFoster and Associates

MC Monte Carlo

MCNP Monte Carlo N-Particle

MIRTE Matériaux en Interaction et Réflexion Toutes Epaisseurs

MSR Molten Salt Reactor

NRAD Neutron Radiography

PWR Pressurized Water Reactor

TRISO Tri-Isotropic