



HAL
open science

Assessment of natural radioactivity and its radiological hazards in several types of cement used in Senegal

Ousmane Ndour, Coumba Thiandoume, Alassane Traore, Xavier Cagnat, Papa Mbaye Diouf, Maurice Ndeye, Ababacar Sadikhe Ndao, Adams Tidjani

► **To cite this version:**

Ousmane Ndour, Coumba Thiandoume, Alassane Traore, Xavier Cagnat, Papa Mbaye Diouf, et al.. Assessment of natural radioactivity and its radiological hazards in several types of cement used in Senegal. SN Applied Sciences, 2020, 2 (12), pp.2078. 10.1007/s42452-020-03904-7 . irsn-04660085

HAL Id: irsn-04660085

<https://irsn.hal.science/irsn-04660085>

Submitted on 23 Jul 2024

HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.



Research Article

Assessment of natural radioactivity and its radiological hazards in several types of cement used in Senegal



Ousmane Ndour¹  · Coumba Thiandoume¹ · Alassane Traore² · Xavier Cagnat³ · Papa Mbaye Diouf¹ · Maurice Ndeye⁴ · Ababacar Sadikhe Ndao² · Adams Tidjani¹

Received: 28 August 2020 / Accepted: 18 November 2020 / Published online: 25 November 2020
© Springer Nature Switzerland AG 2020

Abstract

In this study, the activity concentrations of ^{226}Ra , ^{232}Th and ^{40}K in twenty cement samples of four types (CEM, CEM II, CEM III, and CEM IV) collected from building material suppliers in Senegal were measured using a low-background digital gamma-ray spectrometer equipped with broad energy germanium detector. The activity concentrations of ^{226}Ra , ^{232}Th and ^{40}K varied from 7.1–150.3 Bq kg⁻¹, 3.7–16.1 Bq kg⁻¹, and 48.7–133.9 Bq kg⁻¹, respectively. Also, possible radiological risks from the usage of these materials were assessed by estimating external and internal index, indoor absorbed gamma dose rate and the corresponding annual effective dose, effective dose rate to different body organs and tissues, and excess lifetime cancer risk. The estimated radiological hazard indices were revised in light of the relevant national and international legislation and guidance. The values of the radiological hazard indices were found to be within relevant all limit values for structural building materials.

Keywords Natural radionuclides · Gamma-ray spectrometry · Activity concentrations · radiological hazards indices · Cement

1 Introduction

Humans are continuously exposed to natural radiation which comes from cosmogenic radionuclides and primordial radionuclides [1]. The cosmogenic radionuclides are continuously produced in the upper part of the atmosphere by the interaction of the cosmic radiation with atoms or molecules. The primordial radionuclides are the uranium series with as parent the ^{238}U , ^{235}U series or actinium series, thorium (^{232}Th) series, and ^{40}K which is a non-series of disintegration. When dealing with naturally occurring radioactive material (NORM), only the primordial radionuclides are of radiological interest. Depending on the geological origin of the raw materials (rocks, soil, and industrial products), the building materials may

contain different amounts of natural radionuclides [2, 3]. As cement is most used in building material, it can become a health and environmental problem for the population. According to Mansoor et al., individuals spend 80% of their time at home or office indoor [4]. It is then important to estimate the natural radioactivity in cement.

There are different exposition ways of humans by radionuclides content in cement: internal and external exposure. Internal exposure is due to the inhalation of radon (^{222}Rn) which emanates from the building material [5]. During the inhalation, radon may decay in the track respiratory conducting to the deposition of its progenies and becomes a permanent source of internal exposure [6]. External exposure is due to the emission of γ -rays by

✉ Ousmane Ndour, ousmanendour9031@gmail.com | ¹Natural and Artificial Radiation Laboratory, Department of Physics, Cheikh Anta Diop University, Dakar, Senegal. ²Institute of Applied Nuclear Technology, Cheikh Anta Diop University, Dakar, Senegal. ³Nuclear Safety and Radiation Protection Institute, Orsay, France. ⁴Carbon-14 Laboratory, Cheikh Anta Diop University, Dakar, Senegal.



primordial radionuclides (^{226}Ra , ^{232}Th , and their daughters and ^{40}K).

In Senegal, there are three factories of cement, but so far, no data concerning natural radioactivity of cement used are available. To fill this gap, the main objectives of this study are to assess the ^{226}Ra , ^{232}Th , and ^{40}K activity concentrations and the radiological hazards in the types of cement used as a building material.

2 Materials and methods

2.1 Sample collection and preparation

Twenty cement samples were collected from building material suppliers and labeled properly. The net weight of the collected samples was 1 kg. The gray samples were manufactured by three different domestic cement factories (CEM I, CEM II, and CEM III). To remove moisture, the collected samples were dried at 105 °C for 24 h and then transferred to 60 mL of cylindrical containers with an internal diameter of 72 mm.

2.2 Gamma-ray spectrometry

The ^{226}Ra , ^{232}Th , and ^{40}K activity concentrations were measured using a calibrated broad energy germanium (BEGe) detectors with a relative efficiency of 50% at 1332 keV and an energy resolution of 0.7 keV for 60 keV and 1.8 keV for 1332 keV gamma-rays for ^{241}Am and ^{60}Co , respectively. The detectors were calibrated to energy and efficiency using a mixed radionuclides standard containing ^{241}Am , ^{210}Pb , ^{139}Ce , ^{137}Cs , ^{113}Sn , ^{109}Cd , ^{88}Y , ^{85}Sr , ^{60}Co , ^{57}Co , and ^{51}Cr . The sample analysis was conducted by Genie 2000 software program. The samples were measured at least 80,000 s. As in a planar BEGe detector, the sample is placed on the top of the detector, the coincidences summing were corrected using correction factors calculated by the Monte Carlo simulation, using the GESPECOR software package. For self-attenuation correction, a transmission bench was used for the low energies (below 100 keV). The principle of transmission bench consists to detect gamma-rays emitted by a collimated source of ^{133}Ba and ^{109}Cd passing through a container, then a sample within its container. A schematic diagram of the transmission bench is shown in Fig. 1.

The attenuation coefficient (μ_i) was calculated following the Beer–Lambert equation:

$$N = N_0 e^{-\mu \rho x} \tag{1}$$

where N , N_0 , ρ , and x represent, respectively, the number of photons having passed through the sample within the

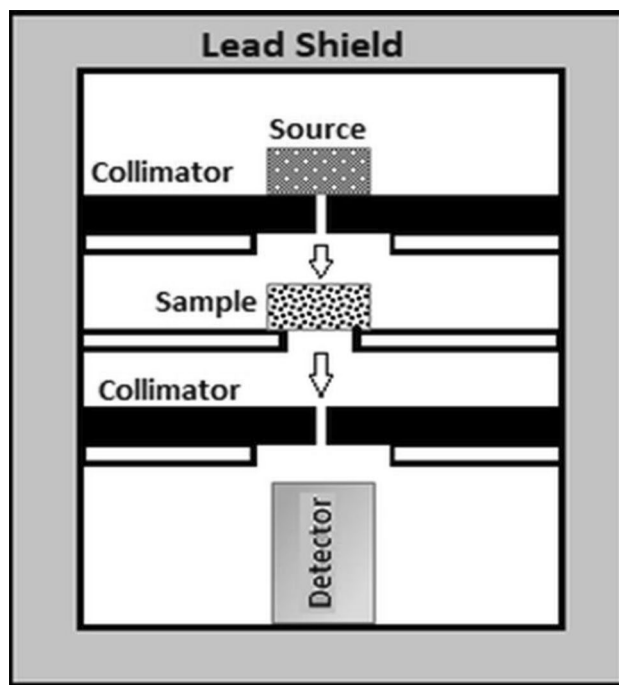


Fig.1 Diagram of transmission bench

geometry, the number of photons detected after crossing the empty geometry, the sample density, and the thickness.

The self-attenuation correction factor (F_{att}) was calculated using the following equation:

$$F_{att} = \frac{1 - e^{-\mu \rho x}}{\mu \rho x} \tag{2}$$

where x , μ , and ρ represent the thickness of the sample, the coefficient of attenuation, and the density, respectively.

As the matrix and the density of the measured samples were different from that of the calibration source, the self-attenuation of the measured samples and the calibration source is therefore different. The relative self-attenuation correction factor $FC_{self}(E)$ is determined by the ratio of the self-attenuation correction factor of the sample to that of the calibration source.

$$FC_{self}(E) = \frac{F_{att.sam}}{F_{att.ref}} \tag{3}$$

where $F_{att.sam}$ and $F_{att.ref}$ are the self-attenuation correction factors of the sample the calibration source, respectively.

The self-attenuation correction factors calculated for ten energies from the transmission source according to their energies were plotted. The interpolated curve obtained was used to calculate the self-attenuation correction factor at other energies.

The ^{226}Ra activity concentration has been estimated using the 186.2 keV gamma-ray. Since the ^{235}U energy peak at 163 keV has not been identified, the gamma-ray interference between ^{226}Ra at 186.2 keV with a peak of ^{235}U at 185.7 keV was resolved taking into account the ratio of $^{238}\text{U}/^{235}\text{U} = 21.7$ and the full energy peak of ^{234}Th at 63.3 keV [7]. The activity concentration of ^{232}Th was estimated using the full energy peaks of ^{228}Ac at 911.2 keV and ^{208}Tl at 583.2 keV taking into account the branching ratio. For ^{40}K activity concentration calculation, its peak at 1460.8 keV was used. The following equation was used to calculate the activity concentration of each radionuclide:

$$A(\text{Bqkg}^{-1}) = \frac{N_{\text{net}}}{P(E_i) \times \epsilon(E_i) \times t \times m \times F_c} \quad (4)$$

where N_{net} represents the net counts under the full absorption peak, $P(E_i)$ the emission intensity, $\epsilon(E_i)$ the detector efficiency at energy E_i , t the counting time, m the sample mass, and F_c the corrective factors taking into account the radioactive decay, the self-attenuation, and the coincidence summing.

2.3 Dose parameters and radiological hazards indices

2.3.1 Absorbed gamma dose rate

At a height of 1 m above the ground, the indoor absorbed gamma dose rate (D) due to γ -ray emitted by ^{226}Ra , ^{232}Th , and ^{40}K is evaluated by the following equation [8, 9]:

$$D(\text{nGyh}^{-1}) = 0.92A_{\text{Ra-226}} + 1.1A_{\text{Th-232}} + 0.08A_{\text{K-40}} \quad (5)$$

The conversion coefficients of ^{226}Ra , ^{232}Th , and ^{40}K activity concentrations into dose for materials used as building materials are 0.92, 1.1, and 0.08 in $\text{nGy h}^{-1}/\text{Bq kg}^{-1}$, respectively. These conversion coefficients were calculated by the Monte Carlo method using a standard room model of 2.8 m \times 4 m \times 5 m in which the wall width is 20 cm and the density 2.35 g.cm^{-3} [10].

2.3.2 Annual effective dose equivalent

The annual effective dose equivalent (AEDE) was calculated by the following equation [10]:

$$\text{AEDE}(\mu\text{Svy}^{-1}) = D(\text{nGyh}^{-1}) \times 0.7(\text{SvGy}^{-1}) \times 0.8 \times 8760\text{hy}^{-1} \times 10^{-3} \quad (6)$$

The conversion coefficient of absorbed dose to an effective dose and the indoor occupancy factor used for the calculation of AEDE were 0.7 Sv Gy^{-1} and 0.8, respectively [10].

2.3.3 Annual gonadal dose equivalent

Since the gonads are organs of interest, the annual gonadal dose equivalent (AGDE) was calculated using the following equation [11–14]:

$$\text{AGDE}(\mu\text{Sv.y}^{-1}) = 3.09A_{\text{Ra-226}} + 4.18A_{\text{Th-232}} + 0.314A_{\text{K-40}} \quad (7)$$

2.3.4 Gamma index and alpha index

The gamma index (I_γ) was calculated to find out if the cements had met the safety requirements for building materials by the following equation [2, 8]:

$$I_\gamma = \frac{A_{\text{Ra-226}}}{300} + \frac{A_{\text{Th-232}}}{200} + \frac{A_{\text{K-40}}}{3000} \quad (8)$$

For material used in a bulky amount, the exemption criterion and the upper dose limit are defined. The exemption criterion (0.3 mSv y^{-1}) corresponds to $I_\gamma \leq 0.5$ and the upper dose limit to $I_\gamma \leq 1$, respectively [8].

The alpha index (I_α) corresponding to the excess alpha radiation due to the ^{222}Rn inhalation from cement was calculated using the following equation [15]:

$$I_\alpha = \frac{A_{\text{Ra-226}}}{200} \quad (9)$$

The I_α should not exceed the unity since the radon exhalation from cement could cause an indoor radon concentration greater than 200 Bq m^{-3} [8, 16].

2.3.5 Excess lifetime of cancer risk

The excess lifetime cancer risk (ELCR) was evaluated by the following formula [17, 18]:

$$\text{ELCR} = \text{AEDE} \times \text{RF} \times \text{DL} \quad (10)$$

where RF is the fatal cancer risk per Sievert (0.05 Sv^{-1}) and DL the life duration (70 y).

2.3.6 Effective dose rate to different organs and tissues

The effective dose rate to different organs and tissues (D_{org}) was calculated using the following equation [19, 20]:

$$D_{\text{org}}(\mu\text{Svy}^{-1}) = \text{AEDE} \times \text{CF} \quad (11)$$

Table 1 Conversion coefficient CF for different organs or tissues [19]

Organ or tissue	Averages values of CF
Bone marrow	0.69
Whole-body	0.68
Lungs	0.64
Ovaries	0.58
Testes	0.82

where CF is the conversion coefficient for the organ dose from air dose (Table 1).

3 Results and discussions

3.1 ²²⁶Ra, ²³²Th, and ⁴⁰K activity concentrations

Table 2 reports the range and average of ²²⁶Ra, ²³²Th, and ⁴⁰K activity concentrations in the types of cement. The ²²⁶Ra activity concentration in cement samples varied from 7.09 Bq kg⁻¹ to 150.25 Bq kg⁻¹. The ²³²Th and ⁴⁰K activity concentration in cement samples varied from 3.72 Bq kg⁻¹ to 16.09 Bq kg⁻¹ and from 48.67 Bq kg⁻¹ to 133.89 Bq kg⁻¹, respectively.

As shown in Table 2, the highest average value of the ²²⁶Ra and ²³²Th activity concentrations was found in CEM I. The CEM IV (white cement) presented the lowest average value of activity concentration of these two radionuclides. Unlike the ²²⁶Ra and ²³²Th, the highest average activity concentration of ⁴⁰K was found in CEM IV and the lowest average value in CEM I. To make a comparison between the ²²⁶Ra, ²³²Th, and ⁴⁰K average activity concentrations and the worldwide average values in building materials, their respective ratios were calculated. The worldwide average values used for comparison were 50 Bq kg⁻¹, 50 Bq kg⁻¹, and 500 Bq kg⁻¹, respectively for ²²⁶Ra, ²³²Th, and ⁴⁰K [21, 22]. In gray cements, the ratio ranges from 1.84 to 2.72 for ²²⁶Ra. Therefore, the ²²⁶Ra activity concentration in gray cements was then found two times higher than the worldwide average value. In white cement, the ratio was 0.16.

Table 2 Range and average with their standard deviation (SD) of ²²⁶Ra, ²³²Th, and ⁴⁰K activity concentrations in the types of cement

Activity concentrations in Bq kg ⁻¹		Type of cement*			
		CEM I	CEM II	CEM III	CEM IV
²²⁶ Ra	Range	129.99–150.25	75.36–149.96	66.73–105.17	7.09–9.24
	Average ± SD	135.95 ± 8.19	109.95 ± 28.42	92.17 ± 16.86	8.07 ± 0.81
²³² Th	Range	14.02–16.09	10.15–13.27	10.62–15.04	3.72–5.85
	Average ± SD	15.09 ± 0.83	12.04 ± 1.16	12.24 ± 1.74	4.68 ± 0.78
⁴⁰ K	Range	48.67–66.22	50.29 ± 98.80	52.00–95.72	104.70–133.89
	Average ± SD	59.25 ± 7.26	80.72 ± 18.26	80.07 ± 19.78	118.91 ± 11.88

*CEM I, CEM II, and CEM III: Portland cement composite; CEM IV: white cement

Then, the ²²⁶Ra average activity concentration in white cement was lower than the worldwide average value cited above. The ratio ranges from 0.24 to 0.30 for ²³²Th and from 0.12 to 0.16 for ⁴⁰K in the gray cement. In white cement, the ratios were 0.10 for ²³²Th and 0.24 for ⁴⁰K. The ²³²Th and ⁴⁰K average activity concentrations were then below their worldwide average values in all types of cement.

The ²²⁶Ra, ²³²Th, and ⁴⁰K average activity concentrations in the gray and white cements were also compared with results from other countries (Table 3). The ²²⁶Ra average activity concentration in gray cement was lower than that of Albania [23] and China [24]. It was higher compared to other countries. For ²³²Th, its average activity concentration was below the cited results in other countries. Regarding the average activity concentration of ⁴⁰K, this study was only lower than that of Albania [23]. The ²²⁶Ra and ²³²Th average activity concentrations found in white cement in this study had the lowest values. The result of the ⁴⁰K activity concentration in Malaysia was only greater than this study [25].

3.2 Dose parameters and radiological hazard indices

The dose parameters and radiological hazards indices were evaluated and presented in Table 4.

The average values of the indoor absorbed gamma dose ranged from 22.09 ± 2.10 nGy h⁻¹ (CEM IV) to 146.41 ± 6.98 nGy h⁻¹ (CEM I). The indoor absorbed gamma dose rate in air of the types of cement exceeds the population-weighted average of 84 nGy h⁻¹, except for CEM IV [10]. From Table 5, it can be seen that the average value of AEDE varied from 108.42 ± 10.32 μSv y⁻¹ (CEM IV) to 718.72 ± 34.26 μSv y⁻¹ (CEM I). The average value of AEDE of all types of cement is lower than the permissible limit which is 1000 μSv y⁻¹. Among the natural radionuclides, the principal contributor to the indoor AEDE was the ²²⁶Ra, with a contribution of 84% in gray cement. The ²²⁶Ra was followed by ²³²Th (11%) and ⁴⁰K (5%). In white cement, the principal contributor was ⁴⁰K (43%), followed by ²²⁶Ra (34%) and ²³²Th (23%).

The average value of AGDE of the types of cement ranged from 81.84 ± 7.88 μSv y⁻¹ (CEM IV) to

Table 3 Comparison of ²²⁶Ra, ²³²Th, and ⁴⁰K average activity concentrations of gray and white cements with those obtained in other countries

Type	Country	Activity concentrations in Bq kg ⁻¹			References
		²²⁶ Ra	²³² Th	⁴⁰ K	
Gray cement	Albania	179.7 ± 48.9	55.0 ± 5.8	17.0 ± 3.3	[23]
	Algeria	41 ± 7	27 ± 3	422 ± 3	[26]
	Cameroon	27 ± 4	15 ± 1	277 ± 117	[27]
	China	118.7 ± 14.2	36.1 ± 17.8	444.5 ± 163.1	[24]
	Egypt	36 ± 4	43 ± 2	82 ± 4	[28]
	Ghana	35.94 ± 0.78	25.44 ± 0.80	233 ± 3.95	[6]
	Iraq	24.25 ± 1.45	25.41 ± 1.65	93.17 ± 7.30	[4]
	Laos	41.12 ± 2.44	16.60 ± 2.37	141.48 ± 4.50	[29]
	Morocco	31 ± 5	19 ± 3	238 ± 29	[30]
	Pakistan	25 ± 10	37 ± 9	245 ± 95	[31]
	Turkey	34 ± 4	15 ± 2	220 ± 13	[9]
White cement	Senegal	112.69 ± 26.02	13.12 ± 1.88	73.35 ± 18.12	In this study
	Cote d'Ivoire	18.85 ± 1.68	22.94 ± 1.96	111.10 ± 7.03	[32]
	Egypt	15 ± 3	17 ± 2	10 ± 5	[33]
	Qatar	18.9 ± 0.5	4.9 ± 0.5	62.9 ± 22.6	[34]
	Malaysia	25.3 ± 1.2	23.4 ± 1.2	362.2 ± 6.7	[25]
	Saudi Arabia	28.53 ± 3.75	43.46 ± 2.18	67.38 ± 3.36	[35]
	Senegal	8.07 ± 0.81	4.68 ± 0.78	118.91 ± 11.88	In this study

Table 4 Average with their standard deviation of dose parameters and radiological hazards indices according to the types of cement

		Cement type			
		CEM I	CEM II	CEM III	CEM IV
Dose parameters	<i>D</i> (nGy h ⁻¹)	146.41 ± 6.98	120.85 ± 27.18	104.67 ± 16.42	22.09 ± 2.10
	AEDE (μSv y ⁻¹)	718.72 ± 34.26	593.27 ± 133.43	513.80 ± 80.63	108.42 ± 10.32
	AGDE (μSv y ⁻¹)	501.75 ± 23.15	415.41 ± 41.04	361.11 ± 24.93	81.84 ± 7.88
Radiological hazards indices	<i>I_γ</i>	0.55 ± 0.03	0.45 ± 0.10	0.40 ± 0.06	0.09 ± 0.01
	<i>I_α</i>	0.68 ± 0.04	0.55 ± 0.14	0.46 ± 0.08	0.040 ± 0.004
	ELCR (10 ⁻³)	2.52 ± 0.12	2.08 ± 0.47	1.80 ± 0.28	0.38 ± 0.04

Table 5 Effective dose rate to different organs and tissues according to types of cement

Type of cement	Effective dose rate (mSv y ⁻¹)				
	Lungs	Ovaries	Bone marrow	Testes	Whole-body
CEM I	0.46	0.42	0.50	0.59	0.49
CEM II	0.38	0.34	0.41	0.49	0.40
CEM III	0.33	0.30	0.36	0.42	0.35
CEM IV	0.07	0.06	0.08	0.09	0.07

501.75 ± 23.15 μSv y⁻¹ (CEM I). The average value of AGDE of CEM I, CEM II, and CEM III was higher than the worldwide average value of 300 μSv y⁻¹ calculated by considering a house containing worldwide average activity concentrations of ²²⁶Ra, ²³²Th, and ⁴⁰K in soil [10, 36].

Table 4 shows that the average value of the gamma Index (*I_γ*) and the alpha index (*I_α*) varied from 0.09 ± 0.01 (CEM IV) to 0.55 ± 0.03 (CEM I) and from 0.040 ± 0.004 (CEM IV) to 0.68 ± 0.04 (CEM I), respectively. The *I_γ* in all types of cement was in the range of the exemption criterion (*I_γ* < 0.5) except the CEM I which was slightly greater but below the recommended limit (*I_γ* = 1) [8]. The *I_α* of the types of cement was lower than the recommended limit value of 1 [8].

The ELCR for each type of cement is presented in Table 4 with an average value ranging from (0.38 ± 0.04) 10⁻³ (CEM IV) to (2.52 ± 0.12) 10⁻³ (CEM I). The excess lifetime cancer risk in all types of cement was higher than the worldwide average value which is 0.29 10⁻³ [10]. The values of ELCR equivalent to 1000, 100, 10, and 1 μSv y⁻¹ will increase the risk of developing mortal cancer by 4%, 0.4%, 0.04%, and 0.004%, respectively [37, 38]. Even all ELCR calculated are

higher than the worldwide value, the chances to increase the risks of cancer in life duration remains negligible.

The values of D_{org} evaluated in different types of organs and tissues according to the types of cement shown in Table 5 were less than the set limit. The calculated values of D_{org} showed that the testes were more sensitive to the radiations, and the ovaries were less sensitive.

3.3 Statistical analysis

3.3.1 Descriptive statistics

A descriptive statistics was performed to describe and also to have a better understanding of the statistical characteristic of the activity concentrations of the natural radionuclides (^{226}Ra , ^{232}Th , and ^{40}K). As the ^{226}Ra and ^{232}Th activity concentrations in white cement samples are found very low compared to gray cements, then they cause a large deviation of the distribution of the activity concentrations. Therefore, they are not used for the statistical analysis of the data. The results of the statistical analysis are reported in Table 6.

The skewness, kurtosis, and the p value using the Shapiro–Wilks test were calculated to have a comprehensive understanding of the distribution of the data. The skewness characterizes the degree of asymmetry of the data [39]. In the theory of probability for a normal distribution, the skewness is equal to zero [40]. However, the data points are not always perfectly symmetric. The absolute magnitude of the ratio between the skewness and its standard error was calculated. If the ratio is less than two, the probability distribution can be assumed to be normally distributed. The distributions of ^{232}Th and

^{40}K activity concentrations in this study had a weak positive skewness, whereas a weak negative skewness was observed for the distribution of ^{226}Ra activity concentration. The ratios between the skewness and its standard error of the distributions of ^{226}Ra , ^{232}Th and ^{40}K activity concentrations were found lower than two.

The kurtosis measures the extent of which data points cluster around the center of the distribution. For a normal distribution, the kurtosis is equal to zero. Negative kurtosis indicates that the data points are less clustered around the center, and the distribution has a thicker tail [41]. Unlike a negative kurtosis, the data points are clustered around the center of the distribution for a positive kurtosis and a thinner tail can be observed [41]. The ratio between the absolute magnitude and the standard error of the kurtosis must be less than two for a normal distribution. These ratios were found less than two for the distributions of ^{226}Ra , ^{232}Th , and ^{40}K activity concentrations.

The Shapiro–Wilks was also used to test the normality of the data. In the Shapiro–Wilks test, if the p value is less than or equal to 0.05, the distribution will not be normal. The found results in Table 3 show that the p values were greater than 0.05 for the distributions of ^{226}Ra , ^{232}Th , and ^{40}K activity concentrations.

The calculated values of the skewness, the kurtosis, and the p value found by the Shapiro–Wilks test showed that the ^{226}Ra , ^{232}Th , and ^{40}K activity concentrations can be assumed normally distributed.

3.3.2 Pearson correlation

Pearson correlation analysis was performed to determine the interdependency and the strength of the relation between the natural radionuclides (^{226}Ra , ^{232}Th , and ^{40}K) in cement samples. The results of the Pearson correlation analysis are shown in Table 7. Between ^{226}Ra and ^{40}K , a weak negative correlation was observed, whereas a high positive correlation was observed between ^{226}Ra and ^{232}Th . It indicates that ^{226}Ra and ^{232}Th have a common source which in general due to the mineralogical components [42]. A high negative correlation was found between ^{232}Th and ^{40}K which can be due to the mineral composition in cement that can affect the mobility of radionuclides [42].

Table 6 Descriptive statistics of ^{226}Ra , ^{232}Th , and ^{40}K activity concentrations in cement samples

	Activity concentration in Bq kg ⁻¹		
	²²⁶ Ra	²³² Th	⁴⁰ K
Arithmetic mean ± MSD*	112.69 ± 6.72	13.12 ± 0.48	73.35 ± 4.68
Standard deviation	26.02	1.88	18.12
Geometric mean	109.67	12.99	71.21
Min	66.73	10.15	48.67
25th percentile	96.48	11.74	57.76
Median	115.23	12.73	66.39
75th percentile	132.24	14.80	89.78
Max	150.25	16.09	98.80
Skewness	-0.24	0.08	0.04
Kurtosis	-0.90	-1.19	-1.68
Shapiro–Wilks test (p value)	0.65	0.64	0.10

*MSD Mean Standard Deviation

Table 7 Pearson correlation matrix for variables

Variables	²²⁶ Ra	²³² Th	⁴⁰ K
²²⁶ Ra	1		
²³² Th	0.60	1	
⁴⁰ K	-0.23	-0.76	1

4 Conclusion

The ^{226}Ra , ^{232}Th , and ^{40}K activity concentrations were assessed in different types of cement available in Senegal by gamma-ray spectrometry. All activity concentrations were less than the worldwide values except the ^{226}Ra in the gray cement. The R_{aeq} was found less than the recommended value. The absorbed dose rate was greater than the worldwide average value of 84 nGy h^{-1} only in the gray cement. The AEDE was less than the recommended limit of 1 mSv y^{-1} . In the CEM I, CEM II, and CEM III, the AGDE was higher compared to the worldwide average of $300 \mu\text{Sv y}^{-1}$. The I_{γ} of CEM I was only greater than the exemption criterion, but it was found below the recommended limit. The I_{α} was slightly greater than the recommended exemption level value in the CEM I and CEM II. However, the alpha index of these two types of cement was below the recommended limit which indicates that the concentration of radon will be less than 200 Bq m^{-3} . The calculated ELCR was greater than the worldwide value; however, the chances to increase the risks of cancer in lifetime remain negligible. The absorbed dose rate according to different types of organs or tissues showed that the testes are more radiosensitive and the higher values of different organs or tissues are found in the CEM I. The contribution of the radiological hazard from the cement under this study is not significant. However, the activity concentration of ^{226}Ra was found greater compared to its worldwide average value, which could serve as an alert to the radiation protection authority.

Acknowledgements The author would like to thank the International Atomic Energy Agency (IAEA) for the fellowship grant in the project SEN7005 "Supporting National Capabilities in Radioanalytical and Radiation Metrology Methods and Techniques". The author thanks also the Metrology of Environmental Radioactivity Laboratory (LMRE) of the Nuclear Safety and Radiation Protection Institute (IRSN) to have accepted to welcome the fellowship with the help of the European Nuclear Safety Training and Tutoring Institute (ENSTTI).

Compliance with ethical standards

Conflict of interest On behalf of all authors, the corresponding author states that there is no conflict of interest.

References

- Bramha S, Sahoo SK, Subramanian V et al (2019) Application of multivariate technique to evaluate spatial distribution of natural radionuclides along Tamil Nadu coastline, east coast of India. *SN Appl Sci* 1:689
- Ešťoková A, Palaščáková L (2013) Assessment of natural radioactivity levels of cements and cement composites in the Slovak Republic. *Int J Environ Res Public Health* 10:165–1719
- Senthilkumar G, Ravisankar R, Vanasundari K et al (2013) Assessment of radioactivity and the associated hazards in local cement types used in Tamilnadu, India. *Radiat Phys Chem* 88:45–48
- Mansoor ZA, Nafae TM, Jelaot AKK (2018) Assessment of natural radioactivity levels and radiological hazards of cement in Iraq. *Nucl Sci* 3:23
- Damla N, Cevik U, Kobya AI, Kobya A et al (2010) Radiation dose estimation and mass attenuation coefficients of cement samples used in Turkey. *J Hazard Mater J* 176:644–649
- Kpeglo DO, Lawluvi H, Faanu A et al (2011) Natural radioactivity and its associated radiological hazards in Ghanaian cement natural radioactivity and its associated radiological hazards in Ghanaian cement. *Res J Environ Earth Sci* 3:161–167
- IAEA (2011) Analytical methodology for the determination of radium isotopes in environmental samples. IAEA analytical quality in nuclear applications series no. 19
- EC-European Commission (1999) Radiological protection principles concerning the natural radioactivity of building materials. *Radiat Prot* 112:1–16
- Özdiş BE, Çam NF, Canbaz Öztürk B (2017) Assessment of natural radioactivity in cements used as building materials in Turkey. *J Radioanal Nucl Chem* 311:307–316
- UNSCEAR (2000) United nations committee on the effect of atomic radiation sources, effects and risks of ionizing radiation. Report to the general assembly, Annex B. United Nations, NewYork
- Mamont-Ciesla K, Gwiazdowski B, Biernacka M, Zak A (1982) Radioactivity of building materials in Poland. In: Vohra G, Pillai KC, Sadavisan S (eds) *Natural radiation environment*. Halsted Press, NewYork, p 551
- UNSCEAR (1988) United nations committee on the effect of atomic radiation sources, effects and risks of ionizing radiation. Report to the general assembly, Annex A. United Nations, NewYork
- Issa S, Mostafa AMA (2015) Distribution of natural radionuclide and radiation hazards of building materials used in Assiut, Egypt. *Int J Bio-Sci Bio-Technol* 7:115–130
- El-Gamal H, Sidique E, El-Haddad M, Farid MEA (2018) Assessment of the natural radioactivity and radiological hazards in granites of Mueilha area (South Eastern Desert, Egypt). *Environ Earth Sci* 77:691
- Righi S, Bruzzi L (2006) Natural radioactivity and radon exhalation in building materials used in Italian dwellings. *J Environ Radioact* 88:158–170
- Viruthagiri G, Rajamannan B, Jawahar KS, Nagar A (2013) Radioactivity and associated radiation hazards in ceramic raw materials and end products. *Radiat Prot Dosim* 157:383–391
- ICRP (1990) Recommendations of the international commission on radiological protection. *Ann ICRP* 21:1–3
- Isinkaye MO, Emelue HU (2015) Natural radioactivity measurements and evaluation of radiological hazards in sediment of Oguta Lake, South East Nigeria. *J Radiat Res Appl Sci* 8:459–469
- Darwish DAE, Abul-nasr KTM, El-khayatt AM (2014) The assessment of natural radioactivity and its associated radiological hazards and dose parameters in granite samples from South Sinai. *J Radiat Res Appl Sci* 8:17–25
- Brien KO, Sanna R (1976) The distribution of absorbed dose-rates in humans from exposure to environmental gamma rays. *Health Phys* 30:71–78
- NEA-OECD (1979) Exposure to radiation from the natural radioactivity in building materials Report by an NEA group of experts of the OECD. Nuclear Energy Agency, Paris
- UNSCEAR (1993) Sources and effects of ionising radiation report to the general assembly, Annex B. United Nations, NewYork

23. Xhixha G, Ahmeti A, Bezzon GP et al (2013) First characterisation of natural radioactivity in building materials manufactured in Albania. *Radiat Prot Dosim* 155:217–223
24. Lu X, Chao S, Yang F (2014) Determination of natural radioactivity and associated radiation hazard in building materials used in Weinan, China. *Radiat Phys Chem* 99:62–67
25. Yasir MS, Ab Majid A, Yahaya R (2007) Study of natural radionuclides and its radiation hazard index in Malaysian building materials. *J Radioanal Nucl Chem* 273:539–541
26. Amrani D, Tahtat M (2001) Natural radioactivity in Algerian building materials. *Appl Radiat Isot* 54:687–689
27. Ngachin M, Garavaglia M, Giovani C et al (2007) Assessment of natural radioactivity and associated radiation hazards in some Cameroonian building materials. *Radiat Meas* 42:61–67
28. El-Taher A (2009) Gamma spectroscopic analysis and associated radiation hazards of building materials used in Egypt. *Radiat Prot Dosim* 138:166–173
29. Xayheungsy S, Khiem LH, Nam LD (2018) Assessment of the natural radioactivity and radiological hazards in Lao cement samples. *Radiat Prot Dosim* 181(3):208–213
30. Kassi B, Boukhair A, Azkour K et al (2018) Assessment of exposure due to technologically enhanced natural radioactivity in various samples of moroccan building materials. *World J Nucl Sci Technol* 8:176–189
31. Faheem M, Mujahid SA, Matiullah M (2008) Assessment of radiological hazards due to the natural radioactivity in soil and building material samples collected from six districts of the Punjab province-Pakistan. *Radiat Meas* 43:1443–1447
32. Alain MG, Huberson GBDL, Florentin BA et al (2019) Assessment of equivalent radium activity and annual effective dose due to building materials in cote d’ivoire by gamma spectrometry: cases of cement. *Open J Appl Sci* 9:774–783
33. Mahmoud KR (2007) Radionuclide content of local and imported cements used in Egypt. *J Radiol Prot* 27:69–77
34. Al-Sulaiti H, Alkhomashi N, Al-Dahan N et al (2011) Determination of the natural radioactivity in Qatari building materials using high-resolution gamma-ray spectrometry. *Nucl Instrum Methods Phys Res Sect A Accel Spectrom Detect Assoc Equip* 652:915–919
35. Al-zahrani J, El-taher A (2017) Natural radioactivity levels and elemental analysis of cement by gamma-ray spectrometer and neutron activation analysis. *Am Sci Res J Eng Technol Sci* 30:173–183
36. Zaidi JH, Arif M, Ahmad S et al (1999) Determination of natural radioactivity in building materials used in the Rawalpindi/Islamabad area by γ -ray spectrometry and instrumental neutron activation analysis. *Appl Radiat Isot* 51:559–564
37. Abdullahi S, Ismail AF, Samat S (2019) Determination of indoor doses and excess lifetime cancer risks caused by building materials containing natural radionuclides in Malaysia. *Nucl Eng Technol* 51:325–336
38. Gad A, Saleh A, Khalifa M (2019) Assessment of natural radionuclides and related occupational risk in agricultural soil, south-eastern Nile Delta, Egypt. *Arab J Geosci* 12:188
39. Groeneveld RA, Meeden G (1984) Measuring Skewness and Kurtosis. *Stat* 33:391–399
40. Ravisankar R, Vanasundari K, Suganya M et al (2014) Multivariate statistical analysis of radiological data of building materials used in Tiruvannamalai, Tamilnadu, India. *Appl Radiat Isot* 85:114–127
41. Sahu SP, Yadav M, Das AJ et al (2017) Multivariate statistical approach for assessment of subsidence in Jharia coalfields, India. *Arab J Geosci* 10:191
42. Raghu Y, Ravisankar R, Chandrasekaran A et al (2017) Assessment of natural radioactivity and radiological hazards in building materials used in the Tiruvannamalai District, Tamilnadu, India, using a statistical approach. *J Taibah Univ Sci* 11:523–533

Publisher’s Note Springer Nature remains neutral with regard to jurisdictional claims in published maps and institutional affiliations.